APPENDIX I

AIR QUALITY ANALYSIS

MOBILE SOURCE AIR POLLUTION MODELING

HUDSON VALLEY WINE VILLAGE DEVELOPMENT
TOWN OF LLOYD,
ULSTER COUNTY, NEW YORK

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APPENDIX A
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1.0 SUMMARY OF FINDINGS

This air quality analysis has been prepared to provide potential air quality impact information in connection with the proposed Hudson Valley Wine Village Development (the "Project") as further described in the 2011 Draft Environmental Impact Statement. The site is located off of U.S. Route 9W, in the Town of Lloyd, Ulster County, New York.

Carbon monoxide (CO) and inhalable particulate matter ($PM_{2.5}$) concentrations associated with the Project and/or expected growth in the project's vicinity, as outlined in the Traffic Impact Study prepared by John Collins Engineers, PC (JCE) were determined using EPA-approved, line source, air pollution modeling analyses for the selected intersection. The intersection modeled was U.S. Route 9W and Chapel Hill Road and Macks Lane. This is a signalized intersection which will carry the bulk of the project's traffic. The future concentrations will be lower in value than the current CO concentration. The results of the modeling analysis indicate that carbon monoxide concentrations will be equivalent (i.e., any increase will be less than detectable thresholds) in the 2021 build verses the 2021 no build scenario. The predicted CO concentrations will not cause, or contribute to the contravention of applicable air quality standards. In addition, $PM_{2.5}$ values will be well below the EPA standards in the future build and no build conditions. Any roadway improvements and timing modifications associated with the project are sufficient to minimize air quality impacts due to the project. A detailed discussion of the air pollution modeling is provided in this report. The modeling was based on the results of analysis of peak PM traffic combined with worst case meteorological conditions at the subject intersection.

2.0 INTRODUCTION

B. Laing Associates, Inc. was retained to prepare an air quality analysis for mobile sources of air pollution (i.e., motor vehicles) associated with the proposed project given a 2021 build scenario. B. Laing Associates, Inc. has provided the following air quality modeling based upon traffic analyses conducted by John Collins Engineers, P.C. at the intersection of U.S. Route 9W and Chapel Hill Road/Macks Lane. Inputs and outputs to the air quality modeling analysis are contained in Appendix A of this report

2.1 Ambient Air Quality

Existing air quality is considered relatively good for the Town of Lloyd as is the area north of New York City. For example, particulate matter ($PM_{2.5}$) as measured in Newburgh, New York (the closest monitoring station) has been below the 15 micrograms per cubic meter (ug/m^3) annual mean standard since 2000 and has ranged between 7.9 and 8.6 ug/m^3 for 2009 to 2011. The 3 year average for the 98th Percentile ug/m^3 was well below the 35 ug/m^3 limit at 23 ug/m^3. Lead levels contained in these particulates have been measured in Wallkill with an annual mean of 0.027 ug/m^3 in 2011 versus a standard of 0.15 ug/m^3.

New York State has not adopted standards for particulate matter (PM_{10}). As such, PM_{10} analysis is usually conducted only when a Federally-funded project is proposed as the project itself or contained within the proposed project. PM_{10} is only monitored in the urban areas of New York City, Rochester, and Buffalo within New York State. In 2011, the 24-hour concentration at the Queens College 2 (R&P) station was 47 ug/m^3. This was well below the Federal Air Quality Standard of 150 ug/m^3.

The closest sulfur dioxide (SO_2) monitoring station is at Mt. Ninham in southeast Putnam County. In 2011, three (3) hour averages have peaked at 12.1 and 11.7 ppb versus a standard of 500 ppb and 24 hour averages have peaked at 5.9 ppb versus a standard of 140 ppb.

Nitrogen dioxide (NO_2) levels are not monitored in New York State Department of Environmental Conservation (NYSDEC) Region 3. They are measured at several sites in Region 2 (Bronx, Queens, and Manhattan). In 2011, the annual average of NO_2 at the Botanical Gardens monitoring station was 20.86 ppm, which is below the standard of 53 ppm. Further, the one hour average for the 98th percentile for the last 3 years was 65 ppm which is also below the 75 ppm standard.

Ozone is measured at Valley Central. It is the only pollutant which could exceed its standard in NYSDEC Region 3 (and State-wide). It is formed from the long-term transport of hydrocarbon emissions in the mid-western United States and as such, is not "local" enforcement on emissions issue. The arithmetic annual mean for this pollutant has ranged from 0.026 to 0.031 parts per million (ppm) for the years 2001 to 2011. The fourth highest maximum daily eight hour average was 0.075 ppm in 2010 and so reached

the 0.075 ppm standard. In 2011, the fourth highest maximum daily eight hour average was 0.067 ppm and so did not exceed the 0.075 ppm standard.

Carbon monoxide (CO) levels are not measured in NYSDEC Region 3. The monitoring station, most comparable to the project site is located in Loudonville, New York[1]. Since 2001, the annual arithmetic mean has ranged from 0.3 to 0.5 ppm. The highest one hour value in 2011 was 1.3 ppm versus a standard of 35 ppm. The highest eight hour value was 1.0 ppm versus a standard of 9.0 ppm[2].

2.2 Intersection Selection

The first level of "air quality screening" as provided in NYSDOT's Environmental Procedures Manual is actually a traffic analysis consistent with the Highway Capacity Manual (HCM). This analysis was provided by John Collins Engineers, P.C. and is also Appended to this DEIS. According to the EPM, predictions of CO concentrations for projects requiring a microscale air quality analysis are necessary. CO analysis is often required or conducted to fulfill SEQR's "hard look" standard as CO can be a local pollutant and concentrations usually occur within a small distance of heavily traveled roadways. $PM_{2.5}$ fine particles are also a result of automobiles and so, were also calculated in this analysis. The EPM provides the guidance that intersections be screened for overall Level of Service (LOS). If the LOS is A, B, or C, no further analyses are required. If any signalized intersections have LOS predicted D, E, or F, significant vehicle queueing may occur and further analysis is required. In this case, the intersection of U.S. Route 9W and Chapel Hill Road/Macks Lane was selected for analysis for three reasons:

1. It is signalized and run at a LOS of E and F (worst case).
2. It represents conditions "typical" of the Town of Lloyd.
3. It will handle the majority of the project's traffic.

If this intersection complies with the ambient air quality standards, it is assumed by the NYSDOT EPM that any other intersections would also comply with the standards.

[1] New York City monitoring locations are not appropriate locations for use in the Town of Lloyd as New York City is far more urbanized. However, New York City monitoring locations were used when no closer or more appropriate locations were available.

[2] The modeling ambient levels used were much higher to add to the environmental conservatism of this analysis.

The NYSDEC currently recommends the use of Level II threshold modeling in conformity with the NYSDOT Environmental Procedures Manual. NYSDOT and U.S. EPA have accepted MOBILE6.2 and CAL3QHC as its official models and the MOBILE 6.2 has been modified by NYSDOT to provide emission factor data specific to each NYSDOT region[3]. These programs were used to determine potential air quality impacts on CO and $PM_{2.5}$ levels due to the proposed project at the subject intersections.

2.3 Regional Analysis

If the project would significantly affect traffic conditions over a large area, it is also appropriate to consider regional air quality effects of the project by way of a mesoscale analysis. Such analyses are generally required for projects which include significant construction on or improvements limited access highways (i.e., New York State Thruway, I-87). No such construction will occur in this area for the project (See NYSDOT-EPM Chapter 1.1, page 31 for specific criteria). Thus, no mesoscale analysis is required for or was conducted for the project.

[3] At present, a new 2010 MOVES emission model has been issued by USEPA's technical and has been "noticed" in the Federal Register (CFR) on March 2, 2010. USEPA had announced a three year grace period for implementation from such notice. To-date NYSDOT/NYSDEC have not yet incorporated the modeling into the State Implementation Plan or the EPM for NYS. We will continue to use MOBILE6.2 until such guidance/regulatory transition occurs in NYS.

3.0 AIR QUALITY MODELING METHODOLOGY

3.1 Microscale Dispersion Modeling

The California Department of Transportation, CALINE3 model (as adopted by the Federal Highway Administration) was originally formulated for free flowing highways. It was adapted in the CAL3QHC format to accommodate intersection queuing (i.e., idling vehicles) situations. The CAL3QHC model is designed to estimate the impact of automobile traffic upon carbon monoxide (CO) and particulate matter ($PM_{2.5}$) concentrations at selected receptors located near roadway locations. It receives input from traffic models, on-site measurements and emission calculations. The dispersion model is the Gaussian-based formula with special modifications by the addition of special links to account for determination of signal cycle times, acceleration/deceleration, and queue lengths through application of traffic engineering principles.

Table 1, below identifies the specific inputs that were utilized in modeling the air quality at the three identified intersections. These inputs are described in greater detail below.

TABLE 1 – MODELING INPUT VALUES

Input	Value Used	Source of Value
Emission Rates	Variable – See modeling inputs	NYSDOT EPM website
Mixing Height	1,000 meters	EPM Chapter 1.1, (C)(xii)
Wind Speed	1.0 meters/second	EPM Chapter 1.1 (C)(xi)
Surface Roughness	175 cm	EPM Chapter 1.1C, Table 10, –office equivalent
Traffic Volumes	PM Peak Hour	NPV Traffic Impact Study
Degree Interval	5 degree intervals	EPM Chapter 1.1 (C)(xiii)
Link Length and Queues	1,200 (min) feet from intersection for Free-flow links. CAL3QHC Program for Queue Link Lengths	EPM Chapter 1.1 (c)(i)-1,000 feet required.
Ambient levels CO-(1 hour – 8 hour) $PM_{2.5}$-(24 hour, 1 year)	 CO – 3.10 – 2.20ppm (ex. cond.) CO – 2.93 – 2.08 (2021)[4] $PM_{2.5}$ – 20.80 – 8.60 ug/m^3	EPM Chapter 1.1 (C)(viii) with a roll back calculation.
Stability	5 - Rural	EPM Chapter 1.1 (C)(ix)

[4] The modeling ambient levels used were much higher to add to the environmental conservatism of this analysis.

3.2 Emission Rates

At or near intersections, vehicles are operating in three possible modes; cruise, acceleration-deceleration or idle. Idling emissions, those which occur as cars queue at an intersection, are generally four to five times greater than cruise emissions (per unit length of roadway). Acceleration-deceleration emissions, those produced as cars stop or resume motion, are also greater than cruise emissions (per unit length of roadway). The roadway length over which the pollutants are emitted is variable, and is dependent upon a number of factors including traffic volume, roadway capacity, vehicle speeds, etc. Cruise and idle emissions are calculated by use of the U.S.EPA MOBILE6.2 model as modified by NYSDOT. The NYSDOT emission factors for each modeled year are weighted by the vehicle miles traveled (VMT) mix for the winter period in NYSDOT Region 8.

The vehicle mix is split into eight standard vehicle classes and a total of 27 sub-classes. The percent composition of each class was determined on New York roadways by NYSDOT. In this way, a composite emission factor is obtained for the required speeds and for idling/running vehicles. The composite emission factor is determined by using the percent composition of the vehicle mix and the NYSDOT emission factors for each modeled year. The weighted emission factors are used in CAL3QHC modeling for the CO and $PM_{2.5}$ (see Emission Factor Table 2). Hot start/cold start engine operating percentages were also set at very conservative standard levels (for "rural" collectors) as specified by NYSDOT.

Once emissions are calculated for vehicle population characteristics, they are then assigned to traffic links at 20 mph speeds in the existing condition for Chapel Hill Road/Macks Lane and 40 mph for U.S. Route 9W and same for the 2021 scenario. The local and principal roadways are modeled as line sources produce an environmentally and conservative result. The emission factors links which are then used by the model for calculation of free-flow emissions. Acceleration /deceleration conditions are simulated by decreasing free-flow speeds within the CAL3QHC free-flow links. The second part of CALINE3 was modified to calculate excess emissions. These emissions were defined by their own unique links, which depend on average queue lengths and delay times which are determined from input signalization characteristics, lane volumes and lane capacities. Finally, all of these factors are assembled, along with receptor locations and meteorological data and are input to CAL3QHC to calculate hourly CO and particulate matter ($PM_{2.5}$) concentrations. Eight hour CO concentrations are determined by use of a persistence factor as described in Section 3.5. $PM_{2.5}$ results 24 hour and annual results are also determined by use of a persistence factor as described in Section 3.5. $PM_{2.5}$ results are similarly compiled based on the September 2004 NYSDOT guidance "*Project Level Particular Matter Analysis, Final Policy*" from Chapter 1.2 of the EPM.

3.3 Physical Model Structure

The model was used in this case to analyze one (1) intersection, with three (3) to six (6) phases each. For most phases, at least two approach/departure links were required; one for free-flow (including acceleration/deceleration) and one or two for

queuing. Each combination of phase, approach and/or queue uniquely defines a link in the intersection. In CAL3QHC, a free-flow link is non-directional; consequently a cross intersection consists of four free flow links. Additional, directional links were added to each intersection at idle to simulate queue emissions. The basis of an intersection description in CAL3QHC is a localized coordinate system. The west to east and south to north coordinates (in feet or meters) are input to define the end points of the link center line. Other required inputs include: effective emission height for the link, width of the link, and traffic on the link. The inputs extend back some 1,200 feet from the subject intersections for free-flow links; the CAL3QHC program sets its own queue link lengths. All intersection approaches have been assigned a queue link in the revised modeling.

After the data for free flow-links on each leg of the intersection were input, data for queuing links arriving at the intersections were input. This information is coded in a similar manner, (i.e., endpoints of the center line of the link are derived based on their location on the coordinate axes). In setting up the coordinates for these two different types of links, the free-flow links terminated at the intersection center while the queue links originate at the approach stop line.

As a general rule, receptors close to a roadway with idling vehicles will experience greater CO concentrations. The existence of emissions from cross-streets plus variations in diffusion and wind flow further complicates the modeling scenario. Therefore, receptor locations were also identified on the coordinate axis system; i.e., so many feet or meters east or west and north or south from the origin of the coordinate axes. The vertical coordinate of the receptor location represents the height of the receptor. Receptors used in the model are found in Table 3 along with their descriptions. Receptors were the building lines of existing, physical structures and real or potential, future sidewalks.

NYSDOT guidance calls for a series of “sidewalk” receptors. They do not actually occur in this case but were established in the modeling coordinate structure to meet the EPM guidance. Sidewalk receptors were assigned for each direction in the intersection being analyzed. Unacceptable receptors included locations where vehicle repairs or fueling are conducted. The model accepts a maximum of 60 receptors.

Sensitive receptors include schools, hospitals, retirement communities and the like. The ambient air quality standards were set to protect the public health and welfare, including sensitive individuals. Thus, in the end, all such receptors are subject to the same standards.

3.4 Traffic Information

The peak PM in vehicles per hour for each link as well as the cruise speed (mph) were input into the model. The peak PM traffic was the maximum increase for the project and was assumed to coincide with worst-case methodology. Traffic velocities were set by NYSDOT-EPM values. All other traffic data were determined from John Collins Engineers, P.C. traffic analyses. Traffic volumes in 2011 existing conditions and

2021 build scenarios were calculated from counts, background levels plus the addition of a growth factor for other development in the region[6].

These various traffic parameters were used in the CAL3QHC determination of vehicle emissions operating in the three modes. Vehicle volumes and speeds were utilized in calculating free-flow emissions. Traffic signal characteristics and capacity service volumes were used in calculating the queue length and delay time, which determined the idle emissions.

It should be noted that free flow speeds were set at 20 mph for Chapel Hill Road/Macks Lane and 40 mph for U.S. Route. This provided the highest emission factor per vehicle mile for the mobile segments modeled. The resultant modeled speeds are, however, actually much lower as the vehicles queuing in the intersection are double counted. That is, the queue links physically overlap the free flow links, "double counting" queuing vehicles and so, in an environmentally conservative manner, reducing the effective speeds below the modeled speeds.

3.5 Dispersion Calculations

Emissions for each link were calculated from MOBILE6.2 factors derived by NYSDOT and described in Section 3.2 above. These factors are then input to the U.S.EPA CAL3QHC model to calculate hourly carbon monoxide concentrations at selected receptor locations. In CAL3QHC, the contribution of each small element of roadway to the concentration at a receptor location is calculated as a function of wind direction, wind speed and stability by use of the Gaussian plume formula. The contribution of the entire length of roadway is then obtained by line integration of that expression. In this instance, local, worst case, one-hour meteorological of 1.0 meter per second wind speed and stability class E was used. The worst stability generally occurs during early morning inversion conditions. After sunrise, the atmosphere gains energy and this condition ameliorates, usually within one to two hours. Since weekday peak traffic from the Project occurs in the PM hour and this meteorological condition occurs just before the AM peak hour, the assumption of their coincidence is conservative. The intersection was modeled for wind directions varying every 5 degrees for a 360-degree compass (i.e., 0 degrees, 5 degrees, 10 degrees, 15 degrees etc. to 355 degrees).

The CAL3QHC model calculated a one hour CO or PM increment and, in this case, incorporates a 0.00 ppm ambient. However, an ambient is added to the result. The CO ambient was calculated as provided in NYSDOT's EPM for this Region. $PM_{2.5}$ values were taken from the NYSDEC's Region 3 air quality monitoring station in Newburgh, New York. Therefore, the true peak value of each pollutant is the sum of the contributions from each link plus the ambient. This result is the maximum predicted concentration for the corresponding peak receptor. The results of the PM analyses were also compared to modeling thresholds provided in EPM Chapter 1.2, Section 4. Levels below such thresholds are determined to have no significant potential to impact inhalable

[6] Traffic numbers, as revised in September 2011 to reflect the Town's commentary on the DEIS, were accounted for in the October 2011 modeling described herein.

pm air quality. The result for each receptor at each intersection was compiled into Tables 4and 5, entitled “Air Quality Results,” as provided at the rear of the text.

Since the analysis must determine a differential between build and no-build scenarios for the eight-hour CO standard, a persistence factor of 0.70 (as provided by NYSDOT for Ulster County) was applied to one-hour results above ambient to yield eight hour results en-lieu of the eight-hour modeling. As provided in EPM Chapter 1.2, Table 5, a persistence factor of 0.4 and 0.08 were used to determine the 24-hour and annual $PM_{2.5}$ values, respectively.

4.0 AIR QUALITY MODELING RESULTS

4.1 CAL3QHC Results

The intersection of U.S. Route 9W and Chapel Hill Road/Macks Lane was analyzed in detail for potential air quality impacts. The CAL3QHC model was run for Peak PM conditions for the 2011 existing condition, 2021 no build and the 2021 build for the Hudson Valley Wine Village Development. Peak PM traffic scenarios were analyzed at the subject intersections using worst case meteorology for each condition. Traffic volumes associated with the build scenarios anticipated the full build of the project. A regional growth rate was included by John Collins Engineers, P.C. in the build scenarios as provided in the traffic analysis. That is, the cumulative impacts of the proposed project plus increases in general traffic were included in the traffic analysis. The air quality analyses do likewise.

Analysis results for the modeled receptors are presented in Tables 4 and 5 plus Appendix A. The maximum CO results (with the project constructed) were 3.83 ppm in the one hour scenario and 2.71 ppm in the eight hour scenario in 2021 PM BUILD at a receptor 36, for the analyzed intersection. At the same intersection, the CO results (without the project constructed) were 3.83 ppm in the one hour scenario and 2.71 ppm in the eight hour scenario in 2021 PM NO BUILD at receptor 36. At the same intersection, the CO results (without the project constructed) were 4.30 ppm in the one hour scenario and 3.04 ppm in the eight hour scenario in 2011 PM EXISTING CONDITION at receptor 36. The results of the BUILD and NO BUILD scenarios are less than the EXISTING CONDITION results because the CO emissions rates for vehicles decreases in each future year. This yearly decrease in emissions outweighs the projected vehicle increase and so, the future CO results are less than the EXISTING CONDITION. The emission rates are listed in the Mobile6 CO Emission Factor Table in the NYSDOT EPM. As all results are well below their respective one hour standard of 35 ppm and eight hour standard of 9 ppm, it was thus determined that the project will not significantly impact air quality. The results for the CO modeling are presented in Table 4.

$PM_{2.5}$ results for the 24 hour and annual scenarios for the modeled receptors are presented in Table 5 – "Air Quality Results" at the rear of the text for whole number (arithmetically-rounded) results and Appendix A for real number (calculated to tenths) results. The peak $PM_{2.5}$ results for the 24 hour scenario using the 20.80 ug/m^3 ambient with the project constructed was 21.60 µg/m³ in the 2021 PM BUILD scenario at receptor 45, for the analyzed intersection. The peak $PM_{2.5}$ results for the 1 year scenario using the 8.60 ug/m^3 ambient with the project constructed was 8.76 µg/m³ in the 2021 PM BUILD scenario at receptor 45, for the analyzed intersection. As the results were well below the standard of 35 µg/m³ (98th percentile-24 hour, not to exceed) and 15 µg/m³ (annual) for $PM_{2.5,}$ it was thus determined that the project will not significantly impact air quality.

The $PM_{2.5}$ results were also calculated for and compared to their respective 24-hour and annual "thresholds" for significant impact. For $PM_{2.5}$, these thresholds are 5 µg/m³ on a 24-hour basis and 0.30 µg/m³ on an annual basis. The peak $PM_{2.5}$ 2021 PM BUILD 24-hour threshold result was 0.80 µg/m³ and the peak $PM_{2.5}$ 2021 PM BUILD annual threshold result were 0.16 µg/m³ at U.S. Route 9W and Chapel Hill Road/Macks Lane. As these values were below their respective thresholds, it was determined that the project will not significantly affect air quality with regard to inhalable particulate matter.

5.0 CONSTRUCTION IMPACTS ON AIR QUALITY

5.1 Construction

The short-term use of heavy equipment operations at the site will result in a temporary, minor increase in pollutant emissions from the various equipment used in the construction process for a several year phased duration. However, the major concern during the construction operation will be the control of fugitive dust during site clearing, excavation, demolition and grading operations. Fugitive dust is essentially airborne soil particles caused by heavy equipment operations entraining the soil into the air. To a lesser extent, some fugitive dust emissions will arise from wind erosion of the exposed soil after the groundcover is removed. All construction related air quality impacts will be of relatively short duration and generally not in proximity to public receptors. The phasing of the project will reduce the intensity of any impacts. In addition, best construction management practices will be employed to reduce soil erosion and possible sources of fugitive dust. This generally includes the daily use of water/spray trucks in dry periods, anti-tracking pads at construction entrances and regular sweeping of any public roads in proximity to the project entry.

MOBILE 6.2 EMISSION FACTOR TABLE **CO** NYSDOT REGION 8

Rev: 1/17/2013 SCENARIO: MACKS/9W/CHAPEL HILL

Tech: DMC

		2011 EMISSION FACTOR TABLE				2011 WEIGHTED EMISSION FACTORS			
		IDLE	CRUISE			IDLE	CRUISE		
Veh. Type	**07/08/09**	**0**	**20**	**30**	**40**	**0**	**20**	**30**	**40**
LDGV	0.4803	48.61	4.83	4.40	4.83	23.35	2.32	2.11	2.32
LDGT1	0.0707	43.23	4.51	4.12	4.55	3.06	0.32	0.29	0.32
LDGT2	0.2349	45.96	4.80	4.39	4.86	10.80	1.13	1.03	1.14
LDGT3	0.1081	48.64	4.99	4.56	5.02	5.26	0.54	0.49	0.54
LDGT4	0.0499	49.22	5.06	4.61	5.09	2.46	0.25	0.23	0.25
HDGV2B	0.0102	104.60	11.61	7.55	6.12	1.07	0.12	0.08	0.06
HDGV3	0.0040	129.34	14.36	9.34	7.57	0.52	0.06	0.04	0.03
HDGV4	0.0012	125.82	13.97	9.09	7.36	0.15	0.02	0.01	0.01
HDGV5	0.0016	168.36	18.69	12.16	9.85	0.27	0.03	0.02	0.02
HDGV6	0.0005	212.43	23.58	15.34	12.43	0.11	0.01	0.01	0.01
HDGV7	0.0006	255.41	28.35	18.44	14.95	0.15	0.02	0.01	0.01
HDGV8A	0.0009	338.96	37.63	24.48	19.84	0.31	0.03	0.02	0.02
LDDV	0.0007	6.58	0.81	0.53	0.41	0.00	0.00	0.00	0.00
LDDT12	0.0011	5.08	0.62	0.41	0.32	0.01	0.00	0.00	0.00
LDDT34	0.0110	4.63	0.57	0.37	0.29	0.05	0.01	0.00	0.00
HDDV2B	0.0018	4.36	0.53	0.35	0.27	0.01	0.00	0.00	0.00
HDDV3	0.0013	5.50	0.67	0.44	0.35	0.01	0.00	0.00	0.00
HDDV4	0.0008	10.47	1.29	0.84	0.66	0.01	0.00	0.00	0.00
HDDV5	0.0011	10.23	1.26	0.82	0.64	0.01	0.00	0.00	0.00
HDDV6	0.0008	12.41	1.52	1.00	0.78	0.01	0.00	0.00	0.00
HDDV7	0.0014	14.81	1.82	1.19	0.93	0.02	0.00	0.00	0.00
HDDV8A	0.0038	29.69	3.64	2.38	1.87	0.11	0.01	0.01	0.01
HDDV8B	0.0040	29.41	3.61	2.36	1.85	0.12	0.01	0.01	0.01
HDGB	0.0007	312.90	34.73	22.59	18.31	0.22	0.02	0.02	0.01
HDDBT	0.0013	36.19	4.44	2.90	2.28	0.05	0.01	0.00	0.00
HDDBS	0.0020	18.53	2.27	1.49	1.17	0.04	0.00	0.00	0.00
MC	0.0053	255.18	13.79	8.97	6.44	1.35	0.07	0.05	0.03
	1.00					**49.50**	**4.99**	**4.44**	**4.80**

		2021 EMISSION FACTOR TABLE				2021 WEIGHTED EMISSION FACTORS			
		IDLE	CRUISE			IDLE	CRUISE		
Veh. Type	**07/08/09**	**0**	**20**	**30**	**40**	**0**	**20**	**30**	**40**
LDGV	0.4803	32.56	3.27	2.98	3.32	15.64	1.57	1.43	1.59
LDGT1	0.0707	31.36	3.31	3.02	3.37	2.22	0.23	0.21	0.24
LDGT2	0.2349	33.46	3.54	3.24	3.62	7.86	0.83	0.76	0.85
LDGT3	0.1081	33.47	3.54	3.24	3.62	3.62	0.38	0.35	0.39
LDGT4	0.0499	34.07	3.60	3.30	3.68	1.70	0.18	0.16	0.18
HDGV2B	0.0102	91.44	10.15	6.60	5.35	0.93	0.10	0.07	0.05
HDGV3	0.0040	123.28	13.69	8.90	7.22	0.49	0.05	0.04	0.03
HDGV4	0.0012	123.67	13.73	8.93	7.24	0.15	0.02	0.01	0.01
HDGV5	0.0016	141.12	15.67	10.19	8.26	0.23	0.03	0.02	0.01
HDGV6	0.0005	148.71	16.51	10.74	8.70	0.07	0.01	0.01	0.00
HDGV7	0.0006	174.21	19.34	12.58	10.20	0.10	0.01	0.01	0.01
HDGV8A	0.0009	193.65	21.50	13.98	11.34	0.17	0.02	0.01	0.01
LDDV	0.0007	5.55	0.68	0.45	0.35	0.00	0.00	0.00	0.00
LDDT12	0.0011	2.84	0.35	0.23	0.18	0.00	0.00	0.00	0.00
LDDT34	0.0110	2.66	0.33	0.21	0.17	0.03	0.00	0.00	0.00
HDDV2B	0.0018	1.31	0.16	0.11	0.08	0.00	0.00	0.00	0.00
HDDV3	0.0013	1.57	0.19	0.13	0.10	0.00	0.00	0.00	0.00
HDDV4	0.0008	2.28	0.28	0.18	0.14	0.00	0.00	0.00	0.00
HDDV5	0.0011	2.90	0.36	0.23	0.18	0.00	0.00	0.00	0.00
HDDV6	0.0008	3.25	0.40	0.26	0.20	0.00	0.00	0.00	0.00
HDDV7	0.0014	4.06	0.50	0.33	0.26	0.01	0.00	0.00	0.00
HDDV8A	0.0038	8.01	0.98	0.64	0.50	0.03	0.00	0.00	0.00
HDDV8B	0.0040	6.93	0.85	0.56	0.44	0.03	0.00	0.00	0.00
HDGB	0.0007	206.96	22.97	14.94	12.11	0.14	0.02	0.01	0.01
HDDBT	0.0013	9.41	1.15	0.75	0.59	0.01	0.00	0.00	0.00
HDDBS	0.0020	6.42	0.79	0.51	0.40	0.01	0.00	0.00	0.00
MC	0.0053	255.18	13.79	8.97	6.44	1.35	0.07	0.05	0.03
	1.00					**34.82**	**3.54**	**3.15**	**3.44**

PM 2.5 ULSTER COUNTY 17-Jan-13 SCENARIO: MACKS/9W/CHAPEL HILL

Veh. Type	07/08/09	2011 EMISSION FACTOR TABLE IDLE	CRUISE	2011 WEIGHTED EMISSION FACTORS IDLE	CRUISE
LDGV	0.4803	0.0000	0.0110	0.0000	0.0053
LDGT1	0.0707	0.0000	0.0110	0.0000	0.0008
LDGT2	0.2349	0.0000	0.0110	0.0000	0.0026
LDGT3	0.1081	0.0000	0.0110	0.0000	0.0012
LDGT4	0.0499	0.0000	0.0110	0.0000	0.0005
HDGV2B	0.0102	0.0000	0.0340	0.0000	0.0003
HDGV3	0.0040	0.0000	0.0430	0.0000	0.0002
HDGV4	0.0012	0.0000	0.0450	0.0000	0.0001
HDGV5	0.0016	0.0000	0.0420	0.0000	0.0001
HDGV6	0.0005	0.0000	0.0490	0.0000	0.0000
HDGV7	0.0006	0.0000	0.0570	0.0000	0.0000
HDGV8A	0.0009	0.0000	0.0700	0.0000	0.0001
LDDV	0.0007	0.0000	0.0600	0.0000	0.0000
LDDT12	0.0011	0.0000	0.0790	0.0000	0.0001
LDDT34	0.0110	0.0000	0.0440	0.0000	0.0005
HDDV2B	0.0018	0.9420	0.0410	0.0017	0.0001
HDDV3	0.0013	0.9480	0.0450	0.0012	0.0001
HDDV4	0.0008	0.9810	0.0700	0.0008	0.0001
HDDV5	0.0011	1.0440	0.0690	0.0011	0.0001
HDDV6	0.0008	1.0580	0.1460	0.0008	0.0001
HDDV7	0.0014	1.0320	0.1390	0.0014	0.0002
HDDV8A	0.0038	1.2210	0.2780	0.0046	0.0011
HDDV8B	0.0040	1.0910	0.2150	0.0044	0.0009
HDGB	0.0007	0.0000	0.0590	0.0000	0.0000
HDDBT	0.0013	1.2220	0.3710	0.0016	0.0005
HDDBS	0.0020	1.0510	0.2820	0.0021	0.0006
MC	0.0053	0.0000	0.0210	0.0000	0.0001
	1.00			0.0198	0.0154

Note that MOBILE6.2 only provides idle emission factors for heavy-duty diesel vehicles and heavy-duty diesel buses. The program does not provide idle emission factors for light-duty or heavy-duty gasoline vehicles; EPA recommends that for these vehicles, users should assume that PM idling emissions are zero (email from EPA to NYSDOT dated June 2004). See page 1 of the NYSDOT Mobile6.2 PM10/PM2.5 Emission Factors Table Guidance document located at the following URL: https://www.dot.ny.gov/divisions/engineering/environmental-analysis/repository/pmemiss.pdf.

PM 2.5 ULSTER COUNTY 17-Jan-13

Veh. Type	07/08/09	2021 EMISSION FACTOR TABLE IDLE	2021 EMISSION FACTOR TABLE CRUISE	2021 WEIGHTED EMISSION FACTORS IDLE	2021 WEIGHTED EMISSION FACTORS CRUISE
LDGV	0.4803	0.0000	0.0110	0.0000	0.0053
LDGT1	0.0707	0.0000	0.0110	0.0000	0.0008
LDGT2	0.2349	0.0000	0.0110	0.0000	0.0026
LDGT3	0.1081	0.0000	0.0110	0.0000	0.0012
LDGT4	0.0499	0.0000	0.0110	0.0000	0.0005
HDGV2B	0.0102	0.0000	0.0190	0.0000	0.0002
HDGV3	0.0040	0.0000	0.0240	0.0000	0.0001
HDGV4	0.0012	0.0000	0.0220	0.0000	0.0000
HDGV5	0.0016	0.0000	0.0270	0.0000	0.0000
HDGV6	0.0005	0.0000	0.0320	0.0000	0.0000
HDGV7	0.0006	0.0000	0.0380	0.0000	0.0000
HDGV8A	0.0009	0.0000	0.0490	0.0000	0.0000
LDDV	0.0007	0.0000	0.0330	0.0000	0.0000
LDDT12	0.0011	0.0000	0.0250	0.0000	0.0000
LDDT34	0.0110	0.0000	0.0170	0.0000	0.0002
HDDV2B	0.0018	0.9240	0.0150	0.0017	0.0000
HDDV3	0.0013	0.9240	0.0160	0.0012	0.0000
HDDV4	0.0008	0.9240	0.0190	0.0007	0.0000
HDDV5	0.0011	0.9240	0.0210	0.0010	0.0000
HDDV6	0.0008	0.9240	0.0340	0.0007	0.0000
HDDV7	0.0014	0.9240	0.0340	0.0013	0.0000
HDDV8A	0.0038	0.9240	0.0620	0.0035	0.0002
HDDV8B	0.0040	0.9240	0.0480	0.0037	0.0002
HDGB	0.0007	0.0000	0.0400	0.0000	0.0000
HDDBT	0.0013	0.9240	0.0500	0.0012	0.0001
HDDBS	0.0020	0.9240	0.0520	0.0018	0.0001
MC	0.0053	0.0000	0.0210	0.0000	0.0001
	1.00			0.0169	0.0120

Note that MOBILE6.2 only provides idle emission factors for heavy-duty diesel vehicles and heavy-duty diesel buses. The program does not provide idle emission factors for light-duty or heavy-duty gasoline vehicles; EPA recommends that for these vehicles, users should assume that PM idling emissions are zero (email from EPA to NYSDOT dated June 2004). See page 1 of the NYSDOT Mobile6.2 PM10/PM2.5 Emission Factors Table Guidance document located at the following URL: https://www.dot.ny.gov/divisions/engineering/environmental-analysis/repository/pmemiss.pdf.

TABLE 3
RECEPTORS (WITH CORRESPONDING DESCRIPTIONS)

U.S. Route 9W and Chapel Hill Road/Macks Lane

Receptor Number	Receptor Description
1.	RECP A
2.	RECP B RITE AID
3.	RECP C GOSPEL CHURC
4.	RECP D FOX POOLS
5.	RECP E HOUSE 109
6.	RECP F WAGON WHEELS
7.	RECP G MCCLEAN MOTO
8.	RECP H HOSANNA CHUR
9.	RECP I HOUSE
10.	RECP J HOUSE
11.	RECP K HOUSE
12.	RECP L HOUSE
13.	RECP M HOUSE 117
14.	RECP N HOUSE 119
15.	RECP O HOUSE 121
16.	RECP P HOUSE
17.	RECP Q HOUSE
18.	RECP R HOUSE
19.	RECP S PODIATRIST
20.	RECP T SIDEWALK
21.	RECP U SIDEWALK
22.	RECP V SIDEWALK
23.	RECP W SIDEWALK
24.	RECP X SIDEWALK
25.	RECP Y SIDEWALK
26.	RECP Z SIDEWALK
27.	RECP BB SIDEWALK
28.	RECP CC SIDEWALK
29.	RECP DD SIDEWALK
30.	RECP EE SIDEWALK
31.	RECP FF SIDEWALK
32.	RECP GG SIDEWALK
33.	RECP HH SIDEWALK
34.	RECP II SIDEWALK
35.	RECP JJ SIDEWALK
36.	RECP KK SIDEWALK
37.	RECP LL SIDEWALK
38.	RECP MM SIDEWALK
39.	RECP NN SIDEWALK
40.	RECP OO SIDEWALK
41.	RECP PP SIDEWALK
42.	RECP QQ SIDEWALK
43.	RECP RR SIDEWALK
44.	RECP SS SIDEWALK
45.	RECP TT SIDEWALK
46.	RECP UU SIDEWALK
47.	RECP VV SIDEWALK
48.	RECP WW SIDEWALK
49.	RECP XX SIDEWALK
50.	RECP YY SIDEWALK
51.	RECP ZZ SIDEWALK

TABLE 4 AIR QUALITY RESULTS - CO 1 AND 8 HOUR VALUES

RESULT TABLE 4A - AIR QUALITY RESULTS CO 1 AND 8 HR VALUES

JOB NO: CHZLYD01 Persistence Factor: 0.70 SCENARIO: PM 2011EXISTING CONDITION

Intersection: ROUTE 9W/MACKS/CHAPEL

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result/ 1 hr	0.20	0.40	0.30	0.20	0.40	0.50	1.00	0.30	0.10	0.20	0.20	0.10	0.40	0.40	0.20	0.10	0.10	0.20	0.30	0.90
1 Hour Ambient	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10
1 Hour Result	3.30	3.50	3.40	3.30	3.50	3.60	4.10	3.40	3.20	3.30	3.30	3.20	3.50	3.50	3.30	3.20	3.20	3.30	3.40	4.00
8 Hour Ambient	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20
8 Hour Result	2.34	2.48	2.41	2.34	2.48	2.55	2.90	2.41	2.27	2.34	2.34	2.27	2.48	2.48	2.34	2.27	2.27	2.34	2.41	2.83

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result/ 1 hr	0.80	0.70	0.60	0.20	0.80	0.50	0.60	0.90	0.70	0.50	1.00	0.60	0.60	0.50	0.40	1.20	1.20	1.20	0.40	0.80
1 Hour Ambient	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10
1 Hour Result	3.90	3.80	3.70	3.30	3.90	3.60	3.70	4.00	3.80	3.60	4.10	3.70	3.70	3.60	3.50	4.30	4.30	4.30	3.50	3.90
8 Hour Ambient	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20	2.20
8 Hour Result	2.76	2.69	2.62	2.34	2.76	2.55	2.62	2.83	2.69	2.55	2.90	2.62	2.62	2.55	2.48	3.04	3.04	3.04	2.48	2.76

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result/ 1 hr	0.90	0.80	0.80	0.80	0.70	0.60	0.70	0.60	0.70	0.70	0.70
1 Hour Ambient	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10
1 Hour Result	4.00	3.90	3.90	3.90	3.80	3.70	3.80	3.70	3.80	3.80	3.80

***** New York State carbon monoxide standard (CO) 35ppm - 1 Hour.
***** New York State carbon monoxide standard (CO) 9ppm - 8 Hour.

RESULT TABLE 4B - AIR QUALITY RESULTS CO 1 AND 8 HR VALUES

JOB NO: CHZLYD01 Persistence Factor: 0.70 SCENARIO: PM 2021 BUILD

Intersection: ROUTE 9W/MACKS/CHAPEL

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result/ 1 hr	0.2	0.40	0.30	0.20	0.30	0.40	0.70	0.30	0.10	0.30	0.20	0.10	0.30	0.40	0.40	0.10	0.10	0.20	0.30	0.70
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.13	3.33	3.23	3.13	3.23	3.33	3.63	3.23	3.03	3.23	3.13	3.03	3.23	3.33	3.33	3.03	3.03	3.13	3.23	3.63
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.22	2.36	2.29	2.22	2.29	2.36	2.57	2.29	2.15	2.29	2.22	2.15	2.29	2.36	2.36	2.15	2.15	2.22	2.29	2.57

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result/ 1 hr	0.7	0.60	0.60	0.20	0.70	0.40	0.50	0.90	0.70	0.60	0.80	0.50	0.50	0.60	0.40	0.90	0.90	0.90	0.50	0.70
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.63	3.53	3.53	3.13	3.63	3.33	3.43	3.83	3.63	3.53	3.73	3.43	3.43	3.53	3.33	3.83	3.83	3.83	3.43	3.63
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.57	2.50	2.50	2.22	2.57	2.36	2.43	2.71	2.57	2.50	2.64	2.43	2.43	2.50	2.36	2.71	2.71	2.71	2.43	2.57

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result/ 1 hr	0.8	0.70	0.60	0.70	0.60	0.60	0.60	0.60	0.60	0.60	0.60
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.73	3.63	3.53	3.63	3.53	3.53	3.53	3.53	3.53	3.53	3.53
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.64	2.57	2.50	2.57	2.50	2.50	2.50	2.50	2.50	2.50	2.50

***** New York State carbon monoxide standard (CO) 35ppm - 1 Hour.
***** New York State carbon monoxide standard (CO) 9ppm - 8 Hour.

RESULT TABLE 4C- AIR QUALITY RESULTS CO 1 AND 8 HR VALUES

JOB NO: CHZLYD01 Persistence Factor: 0.70 SCENARIO: PM 2021 NO BUILD

Intersection: ROUTE 9W/MACKS/CHAPEL

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result/ 1 hr	0.1	0.40	0.20	0.20	0.30	0.30	0.60	0.30	0.10	0.20	0.10	0.10	0.20	0.40	0.30	0.10	0.10	0.20	0.20	0.70
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.03	3.33	3.13	3.13	3.23	3.23	3.53	3.23	3.03	3.13	3.03	3.03	3.13	3.33	3.23	3.03	3.03	3.13	3.13	3.63
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.15	2.36	2.22	2.22	2.29	2.29	2.50	2.29	2.15	2.22	2.15	2.15	2.22	2.36	2.29	2.15	2.15	2.22	2.22	2.57

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result/ 1 hr	0.6	0.60	0.50	0.20	0.70	0.40	0.40	0.60	0.50	0.40	0.80	0.40	0.50	0.40	0.30	0.90	0.90	0.90	0.30	0.60
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.53	3.53	3.43	3.13	3.63	3.33	3.33	3.53	3.43	3.33	3.73	3.33	3.43	3.33	3.23	3.83	3.83	3.83	3.23	3.53
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.50	2.50	2.43	2.22	2.57	2.36	2.36	2.50	2.43	2.36	2.64	2.36	2.43	2.36	2.29	2.71	2.71	2.71	2.29	2.50

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result/ 1 hr	0.6	0.70	0.60	0.50	0.60	0.50	0.50	0.50	0.50	0.50	0.50
1 Hour Ambient	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
1 Hour Result	3.53	3.63	3.53	3.43	3.53	3.43	3.43	3.43	3.43	3.43	3.43
8 Hour Ambient	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08	2.08
8 Hour Result	2.50	2.57	2.50	2.43	2.50	2.43	2.43	2.43	2.43	2.43	2.43

***** New York State carbon monoxide standard (CO) 35ppm - 1 Hour.
***** New York State carbon monoxide standard (CO) 9ppm - 8 Hour.

TABLE 5 AIR QUALITY RESULTS - $PM_{2.5}$ 24 HOUR AND ANNUALVALUES

TABLE 5A- CONVERSION TABLE AIR QUALITY PARTICULATE MATTER VALUES

SCENARIO: PM 2011 EXCON PM2.5

Intersection: ROUTE 9W/MACKS/CHAPEL HILL

JOB NO: CHZLYD01

24 Hour Persistence Factor:	0.4
Annual Persistence Factor:	0.08
24 Hour Ambient:	20.80
1 Year Ambient:	8.60

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result	0.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	1.00	2.00
24 Hour Result	20.80	21.20	21.20	21.20	21.20	21.20	21.20	20.80	20.80	21.20	20.80	20.80	21.20	21.20	21.20	20.80	20.80	20.80	21.20	21.60
24 Hr Increment	0.00	0.40	0.40	0.40	0.40	0.40	0.40	0.00	0.00	0.40	0.00	0.00	0.40	0.40	0.40	0.00	0.00	0.00	0.40	0.80
1 Year Result	8.60	8.68	8.68	8.68	8.68	8.68	8.68	8.60	8.60	8.68	8.60	8.60	8.68	8.68	8.68	8.60	8.60	8.60	8.68	8.76
1 Yr Increment	0.00	0.08	0.08	0.08	0.08	0.08	0.08	0.00	0.00	0.08	0.00	0.00	0.08	0.08	0.08	0.00	0.00	0.00	0.08	0.16

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result	1.00	1.00	1.00	1.00	2.00	1.00	1.00	2.00	2.00	1.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
24 Hour Result	21.20	21.20	21.20	21.20	21.60	21.20	21.20	21.60	21.60	21.20	21.60	21.60	21.60	21.20	21.20	21.20	21.20	21.20	21.20	21.20
24 Hr Increment	0.40	0.40	0.40	0.40	0.80	0.40	0.40	0.80	0.80	0.40	0.80	0.80	0.80	0.40	0.40	0.40	0.40	0.40	0.40	0.40
1 Year Result	8.68	8.68	8.68	8.68	8.76	8.68	8.68	8.76	8.76	8.68	8.76	8.76	8.76	8.68	8.68	8.68	8.68	8.68	8.68	8.68
1 Yr Increment	0.08	0.08	0.08	0.08	0.16	0.08	0.08	0.16	0.16	0.08	0.16	0.16	0.16	0.08	0.08	0.08	0.08	0.08	0.08	0.08

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result	1.00	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
24 Hour Result	21.20	21.20	21.60	21.60	21.60	21.60	21.60	21.60	21.60	21.60	21.60
24 Hr Increment	0.40	0.40	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
1 Year Result	8.68	8.68	8.76	8.76	8.76	8.76	8.76	8.76	8.76	8.76	8.76
1 Yr Increment	0.08	0.08	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16

***** Particulate Matter 2.5 standard (PM2.5) 35µg/m³, 98th percentile 24-Hr. Threshold 5.0µg/m³, 24-Hr.

***** Particulate Matter 2.5 standard (PM2.5) 15µg/m³, annual average prior three years. Threshold 0.3µg/m³, annual

TABLE 5B - CONVERSION TABLE AIR QUALITY PARTICULATE MATTER VALUES

SCENARIO: PM 2021 BLD PM2.5

Intersection: ROUTE 9W/MACKS/CHAPEL HILL

JOB NO: CHZLYD01

24 Hour Persistence Factor: 0.4
Annual Persistence Factor: 0.08
24 Hour Ambient: 20.80
1 Year Ambient: 8.60

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result	0.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.00	1.00	0.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	1.00	2.00
24 Hour Result	20.80	21.20	21.20	21.20	21.20	21.20	21.20	21.20	20.80	21.20	20.80	20.80	21.20	21.20	21.20	20.80	20.80	20.80	21.20	21.60
24 Hr Increment	0.00	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.00	0.40	0.00	0.00	0.40	0.40	0.40	0.00	0.00	0.00	0.40	0.80
1 Year Result	8.60	8.68	8.68	8.68	8.68	8.68	8.68	8.68	8.60	8.68	8.60	8.60	8.68	8.68	8.68	8.60	8.60	8.60	8.68	8.76
1 Yr Increment	0.00	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.00	0.08	0.00	0.00	0.08	0.08	0.08	0.00	0.00	0.00	0.08	0.16

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result	1.00	1.00	1.00	0.00	2.00	1.00	1.00	2.00	2.00	1.00	2.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
24 Hour Result	21.20	21.20	21.20	20.80	21.60	21.20	21.20	21.60	21.60	21.20	21.60	21.60	21.60	21.20	21.20	21.20	21.20	21.20	21.20	21.20
24 Hr Increment	0.40	0.40	0.40	0.00	0.80	0.40	0.40	0.80	0.80	0.40	0.80	0.80	0.80	0.40	0.40	0.40	0.40	0.40	0.40	0.40
1 Year Result	8.68	8.68	8.68	8.60	8.76	8.68	8.68	8.76	8.76	8.68	8.76	8.76	8.76	8.68	8.68	8.68	8.68	8.68	8.68	8.68
1 Yr Increment	0.08	0.08	0.08	0.00	0.16	0.08	0.08	0.16	0.16	0.08	0.16	0.16	0.16	0.08	0.08	0.08	0.08	0.08	0.08	0.08

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result	1.00	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
24 Hour Result	21.20	21.20	21.60	21.60	21.60	21.60	21.60	21.60	21.60	21.60	21.60
24 Hr Increment	0.40	0.40	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80
1 Year Result	8.68	8.68	8.76	8.76	8.76	8.76	8.76	8.76	8.76	8.76	8.76
1 Yr Increment	0.08	0.08	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16

***** Particulate Matter 2.5 standard (PM2.5) 35µg/m³, 98th percentile 24-Hr. Threshold 5.0µg/m³, 24-Hr.
***** Particulate Matter 2.5 standard (PM2.5) 15µg/m³, annual average prior three years. Threshold 0.3µg/m³, annual.

TABLE 5C - CONVERSION TABLE AIR QUALITY PARTICULATE MATTER VALUES

SCENARIO: PM 2021 NO BLD PM2.5

Intersection: ROUTE 9W/MACKS/CHAPEL HILL

JOB NO: CHZLYD01

24 Hour Persistence Factor: 0.4
Annual Persistence Factor: 0.08
24 Hour Ambient: 20.80
1 Year Ambient: 8.60

Receptor Number:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Raw Result	0.00	1.00	1.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	1.00	1.00
24 Hour Result	20.80	21.20	21.20	20.80	21.20	21.20	21.20	20.80	20.80	20.80	20.80	20.80	21.20	21.20	21.20	20.80	20.80	20.80	21.20	21.20
24 Hr Increment	0.00	0.40	0.40	0.00	0.40	0.40	0.40	0.00	0.00	0.00	0.00	0.00	0.40	0.40	0.40	0.00	0.00	0.00	0.40	0.40
1 Year Result	8.60	8.68	8.68	8.60	8.68	8.68	8.68	8.60	8.60	8.60	8.60	8.60	8.68	8.68	8.68	8.60	8.60	8.60	8.68	8.68
1 Yr Increment	0.00	0.08	0.08	0.00	0.08	0.08	0.08	0.00	0.00	0.00	0.00	0.00	0.08	0.08	0.08	0.00	0.00	0.00	0.08	0.08

Receptor Number:	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
Raw Result	1.00	1.00	1.00	0.00	2.00	1.00	1.00	1.00	1.00	1.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
24 Hour Result	21.20	21.20	21.20	20.80	21.60	21.20	21.20	21.20	21.20	21.20	21.60	21.20	21.20	21.20	21.20	21.20	21.20	21.20	21.20	21.20
24 Hr Increment	0.40	0.40	0.40	0.00	0.80	0.40	0.40	0.40	0.40	0.40	0.80	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
1 Year Result	8.68	8.68	8.68	8.60	8.76	8.68	8.68	8.68	8.68	8.68	8.76	8.68	8.68	8.68	8.68	8.68	8.68	8.68	8.68	8.68
1 Yr Increment	0.08	0.08	0.08	0.00	0.16	0.08	0.08	0.08	0.08	0.08	0.16	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08

Receptor Number:	41	42	43	44	45	46	47	48	49	50	51
Raw Result	1.00	1.00	1.00	2.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00
24 Hour Result	21.20	21.20	21.20	21.60	21.20	21.20	21.20	21.20	21.60	21.60	21.20
24 Hr Increment	0.40	0.40	0.40	0.80	0.40	0.40	0.40	0.40	0.80	0.80	0.40
1 Year Result	8.68	8.68	8.68	8.76	8.68	8.68	8.68	8.68	8.76	8.76	8.68
1 Yr Increment	0.08	0.08	0.08	0.16	0.08	0.08	0.08	0.08	0.16	0.16	0.08

***** Particulate Matter 2.5 standard (PM2.5) 35µg/m³, 98th percentile 24-Hr. Threshold 5.0µg/m³, 24-Hr.
***** Particulate Matter 2.5 standard (PM2.5) 15µg/m³, annual average prior three years. Threshold 0.3µg/m³, annual.

APPENDIX A

CAL3QHC MODELING INPUTS AND OUPUTS

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'LLOYD WINERY PROPERTY CAL3QHC ANAL.11'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'  -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
```

```
'LLOYD WINERY PROP PM 11 EX COND, NW SIDE'          8  1  0  'C'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   309  49.50  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  117  49.50  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  656 49.50  1600 2 3
  1
'LINK4 ROUTE 9W  NFR'  'AG'    0.    0.  0.   1200.   2339.  4.80  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   205.  4.99  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  840. 4.99  0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1369 49.50  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   1518.  4.80  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
```

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:51:55

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-285.8	-12.0	232.	270.	AG	227.	100.0	.0	24.0	1.08	11.8
2. LINK2 MACKS LN WBQ	53.0	6.0	255.3	6.0	202.	90.	AG	117.	100.0	.0	12.0	1.10	10.3
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-80.3	45.	180.	AG	168.	100.0	.0	36.0	.26	2.3
4. LINK4 US ROUTE 9	.0	.0	.0	1200.0	1200.	360.	AG	2339.	4.8	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	205.	5.0	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	840.	5.0	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	6496.0	6451.	360.	AG	62.	100.0	.0	12.0	1.79	327.7
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	1518.	4.8	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:51:55

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. LINK1 CHAPEL HILL E	90	77	3.0	309	1600	49.50	2	3
2. LINK2 MACKS LN WBQ	90	79	3.0	117	1600	49.50	2	3
3. LINK3 ROUTE 9W NBQ	90	38	3.0	656	1600	49.50	2	3
7. LINK7 ROUTE 9W SBQ	90	42	3.0	1369	1600	49.50	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0

27.	RECP BB SIDEWALK	*	304.0	-22.0	6.0	*
28.	RECP CC SIDEWALK	*	40.0	-122.0	6.0	*
29.	RECP DD SIDEWALK	*	40.0	-204.0	6.0	*
30.	RECP EE SIDEWALK	*	40.0	-286.0	6.0	*
31.	RECP FF SIDEWALK	*	-40.0	-40.0	6.0	*
32.	RECP GG SIDEWALK	*	-40.0	-122.0	6.0	*
33.	RECP HH SIDEWALK	*	-40.0	-204.0	6.0	*
34.	RECP II SIDEWALK	*	-40.0	-286.0	6.0	*
35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:51:55

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
42. RECP QQ SIDEWALK	-122.0	25.0	6.0
43. RECP RR SIDEWALK	-40.0	30.0	6.0
44. RECP SS SIDEWALK	-22.0	-122.0	6.0
45. RECP TT SIDEWALK	-22.0	-204.0	6.0
46. RECP UU SIDEWALK	-22.0	-286.0	6.0
47. RECP VV SIDEWALK	-42.0	600.0	6.0
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.3	.2	.1	.4	.3	.8	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
5.	.0	.1	.0	.1	.3	.5	1.0	.0	.0	.1	.0	.0	.1	.0	.0	.0	.0	.0	.2	.3
10.	.0	.1	.0	.1	.3	.3	.9	.1	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.2	.1
15.	.0	.1	.0	.1	.1	.2	.9	.1	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
20.	.0	.1	.0	.1	.1	.1	.9	.0	.0	.1	.0	.0	.2	.0	.0	.0	.0	.0	.3	.0
25.	.0	.1	.0	.1	.1	.1	.9	.1	.0	.1	.0	.0	.2	.1	.0	.0	.0	.0	.3	.0
30.	.0	.1	.0	.1	.1	.1	.9	.1	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.3	.0
35.	.0	.1	.0	.1	.1	.1	.8	.1	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.3	.0
40.	.0	.1	.0	.1	.1	.1	.7	.1	.0	.1	.0	.0	.1	.1	.1	.0	.0	.0	.2	.0

45.	*	.0	.0	.0	.1	.1	.1	.6	.2	.0	.2	.1	.0	.1	.1	.1	.0	.0	.0	.2	.0
50.	*	.0	.0	.0	.1	.1	.1	.4	.2	.0	.2	.1	.0	.1	.1	.1	.0	.0	.0	.2	.0
55.	*	.0	.0	.0	.1	.1	.1	.4	.3	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.2	.0
60.	*	.0	.0	.0	.1	.1	.1	.3	.3	.0	.1	.1	.0	.1	.1	.1	.0	.0	.0	.2	.0
65.	*	.0	.0	.0	.1	.1	.1	.4	.2	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.2	.0
70.	*	.0	.0	.0	.1	.1	.1	.2	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.2	.0
75.	*	.0	.0	.0	.1	.1	.1	.3	.1	.0	.2	.1	.1	.1	.1	.0	.0	.0	.0	.2	.0
80.	*	.0	.0	.0	.1	.1	.1	.3	.0	.0	.2	.2	.0	.1	.1	.0	.0	.0	.0	.2	.0
85.	*	.0	.0	.0	.2	.1	.1	.3	.0	.0	.2	.1	.0	.1	.1	.0	.0	.0	.0	.2	.1
90.	*	.0	.0	.0	.2	.1	.1	.3	.0	.0	.1	.0	.0	.1	.2	.1	.0	.0	.1	.2	.2
95.	*	.0	.0	.0	.0	.1	.1	.2	.0	.0	.1	.0	.0	.1	.1	.2	.0	.0	.2	.2	.3
100.	*	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.3	.2	.2	.0	.1	.1	.2	.3
105.	*	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.1	.4	.2	.0	.1	.1	.2	.4
110.	*	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.3	.4	.2	.0	.0	.1	.2	.4
115.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.4	.1	.1	.0	.1	.2	.4
120.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.3	.1	.1	.0	.1	.2	.4
125.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.2	.1	.1	.0	.1	.2	.3
130.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.2	.1	.1	.0	.1	.2	.3
135.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.1	.1	.0	.0	.1	.2	.3
140.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.1	.1	.0	.0	.1	.2	.2
145.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.1	.1	.0	.0	.1	.2	.2
150.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.4	.1	.1	.0	.0	.1	.2	.1
155.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.1	.2	.1
160.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.1	.1
165.	*	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.1
170.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.0
175.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.2	.2
180.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.3
185.	*	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.4
190.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.4
195.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.4
200.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.1	.4
205.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.1	.0	.4

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40	
REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51										
210. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.3
215. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.3
220. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.2
225. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.2
230. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.1	.0	.3
235. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.5
240. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.5
245. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.6
250. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.7
255. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.8
260. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.9
265. *	.1	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.7
270. *	.1	.1	.1	.0	.0	.0	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
275. *	.1	.1	.1	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
280. *	.1	.2	.1	.0	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
285. *	.1	.3	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
290. *	.1	.4	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
295. *	.1	.4	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
300. *	.1	.4	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
305. *	.1	.4	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
310. *	.1	.3	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
315. *	.1	.3	.1	.1	.0	.0	.7	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
320. *	.1	.2	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
325. *	.1	.2	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
330. *	.1	.3	.2	.1	.0	.1	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
335. *	.1	.3	.2	.1	.0	.1	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
340. *	.0	.4	.2	.1	.0	.1	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
345. *	.1	.4	.3	.1	.1	.1	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6
350. *	.1	.4	.3	.1	.1	.1	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6
355. *	.0	.3	.3	.1	.3	.3	.8	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6
MAX *	.2	.4	.3	.2	.4	.5	1.0	.3	.1	.2	.2	.1	.4	.4	.2	.1	.1	.2	.3	.9
DEGR. *	240	290	345	85	0	5	5	55	65	45	80	65	115	105	95	115	100	95	20	260

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	.2	.0	.0	.0	.5	.2	.0	.7	.4	.5	.6	.6	.5	.5	.3	1.0	.9	.4	.0	.0
5.	.0	.0	.0	.0	.3	.2	.0	.5	.4	.2	.8	.5	.6	.4	.4	.9	.9	.6	.0	.1
10.	.0	.0	.0	.0	.2	.2	.0	.3	.2	.2	.7	.5	.5	.5	.3	1.0	.9	.7	.0	.1
15.	.0	.0	.0	.0	.1	.2	.0	.1	.1	.1	.7	.5	.5	.4	.2	1.0	.9	.8	.0	.2
20.	.0	.0	.0	.0	.1	.2	.0	.1	.1	.1	.6	.4	.4	.4	.2	1.1	1.0	.9	.0	.2
25.	.0	.0	.0	.0	.1	.2	.0	.1	.1	.1	.5	.3	.3	.3	.2	1.1	1.0	.9	.0	.2
30.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.1	.4	.4	.4	.3	.2	1.1	1.0	1.0	.0	.2
35.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.0	.3	.5	.4	.3	.2	1.1	1.0	.9	.1	.1
40.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.0	.4	.5	.3	.3	.2	1.1	1.1	.9	.1	.1
45.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.0	.2	.4	.3	.2	.1	1.2	1.1	1.0	.1	.1
50.	.0	.0	.0	.0	.3	.2	.0	.1	.0	.0	.2	.4	.2	.1	.1	1.0	1.1	1.0	.1	.1
55.	.0	.0	.0	.0	.3	.1	.0	.1	.0	.0	.3	.4	.2	.1	.1	1.0	1.1	1.1	.1	.1
60.	.0	.0	.0	.0	.3	.1	.0	.1	.0	.0	.2	.3	.1	.1	.1	.9	1.1	1.1	.1	.1
65.	.0	.0	.0	.0	.3	.0	.0	.0	.0	.0	.2	.3	.1	.1	.1	.9	1.1	1.2	.1	.1
70.	.0	.0	.0	.0	.3	.1	.1	.0	.0	.0	.3	.2	.1	.1	.1	.9	1.1	1.2	.1	.1
75.	.0	.0	.0	.0	.3	.1	.1	.0	.0	.0	.4	.1	.1	.1	.1	.8	1.2	1.2	.1	.1
80.	.1	.0	.0	.0	.2	.1	.1	.0	.0	.0	.4	.1	.1	.1	.1	.4	1.0	1.2	.1	.1
85.	.1	.0	.0	.0	.1	.1	.1	.0	.0	.0	.4	.1	.1	.1	.1	.5	.8	.9	.2	.2
90.	.2	.0	.0	.0	.1	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.4	.6	.6	.3	.5
95.	.4	.1	.1	.0	.0	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.3	.3	.3	.4	.6
100.	.5	.2	.1	.1	.0	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.2	.3	.2	.3	.6
105.	.5	.2	.1	.1	.0	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.2	.1	.1	.3	.7
110.	.6	.3	.1	.1	.0	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.2	.1	.0	.2	.8
115.	.5	.2	.0	.0	.0	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.2	.1	.0	.2	.8
120.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.1	.1	.0	.1	.8
125.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.1	.1	.0	.1	.8
130.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.1	.1	.0	.1	.7
135.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.2	.1	.1	.1	.1	.1	.8
140.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.2	.2	.1	.1	.1	.1	.8
145.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.1	.1	.7
150.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.1	.1	.7
155.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.1	.1	.7

160.	*	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.1	.1	.7
165.	*	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.0	.1	.6
170.	*	.3	.3	.0	.0	.1	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.0	.1	.5
175.	*	.3	.3	.0	.0	.2	.0	.0	.1	.1	.1	.2	.2	.2	.2	.2	.1	.0	.0	.1	.4
180.	*	.3	.3	.0	.0	.4	.0	.0	.2	.1	.1	.2	.2	.1	.1	.1	.0	.0	.0	.1	.4
185.	*	.4	.3	.0	.0	.4	.0	.0	.2	.2	.2	.1	.1	.1	.1	.1	.0	.0	.0	.1	.3
190.	*	.4	.3	.0	.0	.5	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2
195.	*	.4	.4	.0	.0	.6	.1	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2
200.	*	.4	.4	.1	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
205.	*	.4	.4	.1	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	.4	.4	.1	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
215.	.4	.4	.1	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
220.	.5	.5	.1	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
225.	.6	.5	.0	.0	.7	.1	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
230.	.6	.5	.0	.0	.6	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
235.	.6	.5	.1	.0	.6	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
240.	.6	.6	.1	.0	.5	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1
245.	.7	.7	.2	.0	.5	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1
250.	.7	.7	.2	.1	.4	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2
255.	.7	.7	.5	.1	.5	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2
260.	.8	.7	.4	.2	.5	.2	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.0	.0	.2	.2
265.	.7	.7	.5	.2	.7	.5	.2	.1	.1	.1	.3	.0	.0	.0	.0	.3	.2	.1	.2	.2
270.	.5	.7	.6	.2	.8	.4	.4	.1	.1	.1	.5	.0	.0	.0	.0	.5	.3	.1	.1	.1
275.	.4	.5	.4	.1	.8	.5	.4	.1	.1	.1	.7	.0	.0	.0	.0	.7	.4	.1	.1	.1
280.	.2	.3	.2	.0	.8	.5	.5	.3	.1	.1	.9	.1	.0	.0	.0	.9	.5	.1	.0	.0
285.	.1	.1	.1	.1	.6	.5	.6	.4	.1	.1	1.0	.2	.0	.0	.0	1.0	.7	.1	.0	.0
290.	.1	.1	.1	.1	.5	.4	.4	.4	.1	.1	1.0	.2	.0	.0	.0	1.0	.8	.1	.0	.0
295.	.2	.1	.1	.1	.5	.4	.3	.5	.2	.1	.9	.3	.0	.0	.0	1.0	.9	.1	.0	.0
300.	.2	.1	.1	.1	.4	.4	.3	.5	.2	.1	.9	.4	.1	.0	.0	1.0	.9	.1	.0	.0
305.	.2	.1	.1	.1	.3	.4	.2	.5	.3	.2	.8	.4	.1	.0	.0	1.0	.9	.1	.0	.0
310.	.2	.1	.1	.1	.3	.4	.2	.5	.3	.2	.7	.3	.1	.0	.0	.9	.9	.1	.0	.0
315.	.2	.1	.1	.1	.2	.4	.1	.4	.4	.3	.7	.3	.2	.1	.0	.9	.9	.1	.0	.0
320.	.2	.2	.1	.1	.2	.5	.1	.5	.4	.4	.6	.3	.2	.1	.0	.8	.8	.1	.0	.0
325.	.3	.2	.1	.1	.4	.5	.1	.5	.4	.4	.5	.3	.2	.1	.0	.8	.8	.1	.0	.0
330.	.3	.2	.1	.0	.4	.5	.1	.5	.3	.3	.5	.3	.2	.2	.0	.8	.8	.1	.0	.0
335.	.3	.2	.2	.0	.5	.5	.2	.5	.3	.3	.4	.3	.2	.2	.0	.8	.8	.1	.0	.0
340.	.3	.2	.2	.0	.5	.4	.2	.7	.5	.4	.3	.2	.2	.2	.1	.8	.8	.2	.0	.0
345.	.3	.2	.2	.0	.6	.4	.2	.8	.5	.5	.2	.2	.2	.2	.1	.7	.7	.2	.0	.0
350.	.3	.2	.1	.0	.6	.4	.1	.9	.5	.5	.4	.4	.3	.3	.1	.7	.7	.3	.0	.0
355.	.2	.1	.1	.0	.6	.3	.1	.7	.7	.5	.5	.4	.4	.3	.4	.8	.7	.3	.0	.0
MAX	.8	.7	.6	.2	.8	.5	.6	.9	.7	.5	1.0	.6	.6	.5	.4	1.2	1.2	1.2	.4	.8
DEGR.	260	245	270	260	270	265	285	350	355	0	285	0	5	0	5	45	75	65	95	135

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	.1	.2	.6	.6	.7	.5	.5	.4	.5	.5	.4
5.	.2	.2	.7	.8	.7	.6	.6	.2	.3	.3	.2
10.	.2	.3	.7	.7	.6	.6	.7	.1	.1	.1	.1
15.	.2	.3	.7	.6	.5	.5	.7	.0	.0	.0	.0
20.	.2	.3	.6	.5	.5	.3	.6	.0	.0	.0	.0
25.	.2	.3	.6	.5	.5	.4	.5	.0	.0	.0	.0
30.	.2	.3	.5	.6	.4	.3	.5	.0	.0	.0	.0
35.	.2	.3	.5	.5	.3	.3	.5	.0	.0	.0	.0
40.	.2	.3	.5	.5	.3	.3	.5	.0	.0	.0	.0
45.	.2	.3	.4	.5	.3	.2	.5	.0	.0	.0	.0
50.	.2	.2	.4	.4	.3	.2	.5	.0	.0	.0	.0
55.	.2	.2	.4	.4	.2	.2	.4	.0	.0	.0	.0
60.	.1	.2	.4	.4	.2	.2	.3	.0	.0	.0	.0
65.	.1	.2	.3	.3	.2	.2	.3	.0	.0	.0	.0
70.	.1	.2	.3	.3	.2	.2	.3	.0	.0	.0	.0
75.	.1	.1	.3	.2	.2	.2	.3	.0	.0	.0	.0
80.	.1	.1	.3	.2	.2	.2	.3	.0	.0	.0	.0
85.	.3	.2	.3	.2	.2	.2	.3	.0	.0	.0	.0
90.	.4	.2	.4	.2	.2	.2	.3	.0	.0	.0	.0
95.	.5	.3	.4	.2	.2	.2	.3	.0	.0	.0	.0
100.	.5	.4	.4	.2	.2	.2	.3	.0	.0	.0	.0
105.	.7	.4	.4	.2	.2	.2	.3	.0	.0	.0	.0
110.	.8	.5	.3	.2	.2	.2	.3	.0	.0	.0	.0
115.	.9	.6	.3	.2	.2	.2	.3	.0	.0	.0	.1
120.	.9	.7	.2	.2	.2	.2	.3	.0	.0	.0	.1
125.	.8	.8	.4	.2	.2	.2	.4	.0	.0	.0	.1
130.	.8	.8	.4	.2	.2	.2	.5	.0	.0	.0	.1
135.	.8	.7	.4	.2	.2	.2	.5	.0	.0	.1	.1
140.	.8	.7	.5	.2	.2	.2	.5	.0	.0	.1	.1
145.	.7	.7	.5	.2	.2	.2	.5	.0	.0	.1	.1
150.	.7	.7	.5	.2	.2	.2	.5	.0	.1	.1	.1
155.	.7	.7	.4	.3	.3	.3	.5	.0	.1	.1	.1

160.	*	.7	.7	.4	.3	.3	.3	.6	.0	.1	.1	.1
165.	*	.7	.7	.4	.3	.3	.3	.6	.0	.1	.1	.1
170.	*	.7	.7	.3	.3	.3	.3	.6	.1	.1	.1	.1
175.	*	.6	.7	.3	.3	.3	.3	.6	.1	.2	.2	.2
180.	*	.6	.6	.3	.3	.2	.2	.5	.4	.3	.2	.2
185.	*	.6	.6	.3	.2	.2	.2	.3	.5	.3	.4	.3
190.	*	.6	.6	.2	.1	.1	.1	.2	.6	.5	.4	.4
195.	*	.6	.6	.3	.0	.0	.0	.1	.6	.7	.5	.4
200.	*	.6	.6	.4	.0	.0	.0	.1	.6	.6	.5	.4
205.	*	.6	.6	.4	.0	.0	.0	.0	.5	.6	.6	.3

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	.6	.6	.5	.0	.0	.0	.0	.4	.6	.6	.3
215.	.6	.7	.5	.0	.0	.0	.0	.4	.5	.6	.4
220.	.7	.7	.6	.0	.0	.0	.0	.4	.5	.6	.6
225.	.7	.7	.6	.0	.0	.0	.0	.4	.5	.6	.6
230.	.7	.7	.7	.0	.0	.0	.0	.4	.5	.6	.6
235.	.6	.7	.7	.0	.0	.0	.0	.4	.4	.5	.7
240.	.6	.8	.7	.0	.0	.0	.0	.3	.4	.5	.7
245.	.5	.8	.8	.0	.0	.0	.0	.3	.4	.4	.6
250.	.5	.8	.7	.0	.0	.0	.0	.3	.4	.4	.6
255.	.4	.7	.8	.0	.0	.0	.0	.3	.4	.4	.5
260.	.3	.6	.7	.0	.0	.0	.0	.3	.4	.4	.4
265.	.3	.5	.4	.0	.0	.0	.0	.3	.4	.4	.3
270.	.1	.2	.3	.0	.0	.0	.0	.3	.4	.4	.3
275.	.1	.2	.2	.0	.0	.0	.0	.3	.4	.4	.3
280.	.0	.0	.0	.1	.0	.0	.0	.3	.4	.4	.3
285.	.0	.0	.0	.2	.0	.0	.0	.3	.4	.4	.3
290.	.0	.0	.0	.3	.0	.0	.0	.3	.4	.4	.3
295.	.0	.0	.0	.3	.0	.0	.0	.3	.4	.4	.3
300.	.0	.0	.0	.4	.1	.0	.0	.3	.4	.4	.3
305.	.0	.0	.0	.4	.1	.0	.0	.4	.4	.4	.3
310.	.0	.0	.0	.3	.2	.1	.0	.4	.4	.4	.4
315.	.0	.0	.0	.3	.2	.1	.0	.4	.4	.4	.4
320.	.0	.0	.0	.3	.2	.1	.0	.4	.4	.4	.4
325.	.0	.0	.0	.3	.2	.2	.0	.4	.4	.4	.4
330.	.0	.0	.0	.3	.2	.2	.0	.4	.5	.5	.4
335.	.0	.0	.0	.2	.2	.2	.0	.4	.5	.5	.4
340.	.0	.0	.0	.2	.2	.2	.0	.5	.6	.6	.5
345.	.0	.0	.0	.2	.1	.1	.0	.6	.7	.7	.6
350.	.0	.0	.2	.3	.3	.3	.2	.6	.7	.7	.6
355.	.0	.1	.4	.5	.5	.5	.3	.5	.6	.6	.5
MAX	.9	.8	.8	.8	.7	.6	.7	.6	.7	.7	.7
DEGR.	115	125	245	5	0	5	10	190	195	345	235

THE HIGHEST CONCENTRATION OF 1.20 PPM OCCURRED AT RECEPTOR REC36.

```
'LLOYD WINERY PROPERTY CAL3QHC ANAL.21'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'  -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
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'LLOYD WINERY PROP PM 21 NO BLD, NW SIDE'          8  1  0  'C'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   327  34.82  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  123  34.82  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  709 34.82  1600 2 3
  1
'LINK4 ROUTE 9W NFR'  'AG'    0.    0.  0.   1200.   2480.  3.44  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   216.  3.54  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  890. 3.54  0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1447 34.82  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   1626.  3.44  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
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JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:55:51

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-381.0	-12.0	327.	270.	AG	160.	100.0	.0	24.0	1.15	16.6
2. LINK2 MACKS LN WBQ	53.0	6.0	319.2	6.0	266.	90.	AG	82.	100.0	.0	12.0	1.16	13.5
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-84.0	49.	180.	AG	118.	100.0	.0	36.0	.28	2.5
4. LINK4 ROUTE 9W	.0	.0	.0	1200.0	1200.	360.	AG	2480.	3.4	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	216.	3.5	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	890.	3.5	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	7292.0	7247.	360.	AG	44.	100.0	.0	12.0	1.89	368.1
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	1626.	3.4	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:55:51

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. LINK1 CHAPEL HILL E	90	77	3.0	327	1600	34.82	2	3
2. LINK2 MACKS LN WBQ	90	79	3.0	123	1600	34.82	2	3
3. LINK3 ROUTE 9W NBQ	90	38	3.0	709	1600	34.82	2	3
7. LINK7 ROUTE 9W SBQ	90	42	3.0	1447	1600	34.82	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0
27. RECP BB SIDEWALK	304.0	-22.0	6.0

28.	RECP CC SIDEWALK	*	40.0	-122.0	6.0	*
29.	RECP DD SIDEWALK	*	40.0	-204.0	6.0	*
30.	RECP EE SIDEWALK	*	40.0	-286.0	6.0	*
31.	RECP FF SIDEWALK	*	-40.0	-40.0	6.0	*
32.	RECP GG SIDEWALK	*	-40.0	-122.0	6.0	*
33.	RECP HH SIDEWALK	*	-40.0	-204.0	6.0	*
34.	RECP II SIDEWALK	*	-40.0	-286.0	6.0	*
35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:55:51

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
42. RECP QQ SIDEWALK	-122.0	25.0	6.0
43. RECP RR SIDEWALK	-40.0	30.0	6.0
44. RECP SS SIDEWALK	-22.0	-122.0	6.0
45. RECP TT SIDEWALK	-22.0	-204.0	6.0
46. RECP UU SIDEWALK	-22.0	-286.0	6.0
47. RECP VV SIDEWALK	-42.0	600.0	6.0
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.3	.2	.0	.2	.3	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.3
5.	.0	.1	.0	.0	.3	.2	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.2
10.	.0	.1	.0	.0	.2	.3	.6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1
15.	.0	.1	.0	.0	.1	.2	.6	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0
20.	.0	.1	.0	.0	.1	.1	.6	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.0
25.	.0	.1	.0	.1	.1	.1	.6	.1	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.0
30.	.0	.1	.0	.1	.1	.1	.6	.2	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
35.	.0	.1	.0	.1	.1	.1	.4	.2	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
40.	.0	.1	.0	.1	.1	.1	.4	.2	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
45.	.0	.1	.0	.1	.1	.1	.4	.3	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0
50.	.0	.0	.0	.1	.1	.1	.3	.2	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0
55.	.0	.0	.0	.1	.1	.1	.2	.2	.0	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0
60.	.0	.0	.0	.1	.1	.1	.2	.2	.1	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0
65.	.0	.0	.0	.1	.1	.1	.1	.2	.1	.1	.0	.0	.1	.0	.0	.0	.0	.0	.1	.0
70.	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.0
75.	.0	.0	.0	.1	.1	.1	.2	.1	.0	.2	.1	.0	.1	.0	.0	.0	.0	.0	.1	.0
80.	.0	.0	.0	.2	.1	.1	.3	.0	.0	.2	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0
85.	.0	.0	.0	.2	.1	.1	.3	.0	.0	.1	.1	.0	.1	.0	.0	.0	.0	.0	.1	.1
90.	.0	.0	.0	.2	.1	.1	.2	.0	.0	.1	.0	.0	.1	.0	.1	.0	.0	.1	.1	.2
95.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.1	.0	.0	.0	.1	.1	.0	.0	.2	.1	.2
100.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.3	.0	.1	.2	.1	.3
105.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.1	.2	.3	.0	.1	.1	.1	.3
110.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.2	.4	.2	.0	.1	.1	.1	.3
115.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.4	.2	.1	.0	.1	.1	.3
120.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.4	.1	.1	.0	.1	.1	.3
125.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.3	.1	.1	.0	.1	.1	.2
130.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.1	.1	.2
135.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.2	.1	.1	.0	.1	.1	.2
140.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.1	.2
145.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.2	.1
150.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.1	.1
155.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.1
160.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.1

165.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.0
170.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.2	.0
175.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.2	.2
180.	*	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.2
185.	*	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.3
190.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.4
195.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.4
200.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.4
205.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.1	.2

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.2
215. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
220. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1
225. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2
230. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2
235. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.0	.0	.0	.0	.2
240. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.4
245. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.5
250. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.6
255. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.7
260. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.7
265. *	.1	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6
270. *	.1	.1	.1	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
275. *	.1	.1	.1	.0	.0	.0	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
280. *	.1	.2	.1	.0	.0	.0	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
285. *	.1	.2	.1	.0	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
290. *	.0	.3	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
295. *	.1	.3	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
300. *	.1	.4	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
305. *	.1	.3	.1	.1	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
310. *	.1	.3	.1	.1	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
315. *	.1	.2	.1	.1	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
320. *	.1	.2	.1	.1	.0	.0	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
325. *	.1	.2	.2	.1	.0	.1	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
330. *	.1	.1	.2	.1	.0	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
335. *	.0	.1	.2	.1	.0	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
340. *	.0	.2	.2	.0	.1	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
345. *	.0	.4	.1	.0	.1	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
350. *	.0	.3	.2	.0	.1	.1	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
355. *	.0	.3	.2	.0	.1	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
MAX *	.1	.4	.2	.2	.3	.3	.6	.3	.1	.2	.1	.1	.2	.4	.3	.1	.1	.2	.2	.7
DEGR. *	235	300	0	80	5	0	10	45	60	75	70	80	110	110	100	115	100	95	10	255

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210. *																				
215. *																				
220. *																				
225. *																				
230. *																				
235. *																				
240. *																				
245. *																				
250. *																				
255. *																				
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265. *																				
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275. *																				
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285. *																				
290. *																				
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310. *																				
315. *																				
320. *																				
325. *																				
330. *																				
335. *																				
340. *																				
345. *																				
350. *																				
355. *																				
MAX *																				
DEGR. *																				

(DEGR)*	REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210. *											
215. *											
220. *											
225. *											
230. *											
235. *											
240. *											
245. *											
250. *											
255. *											
260. *											
265. *											
270. *											
275. *											
280. *											
285. *											
290. *											
295. *											
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310. *											
315. *											
320. *											
325. *											
330. *											
335. *											
340. *											
345. *											
350. *											
355. *											
MAX *											
DEGR. *											

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	.1	.0	.0	.0	.3	.2	.2	.4	.4	.2	.5	.4	.4	.2	.3	.8	.6	.6	.0	.0
5.	.0	.0	.0	.0	.2	.2	.2	.3	.2	.2	.6	.4	.4	.4	.3	.8	.7	.6	.0	.0
10.	.0	.0	.0	.0	.1	.2	.2	.2	.1	.0	.6	.4	.5	.3	.2	.7	.8	.7	.0	.1
15.	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.5	.4	.3	.2	.2	.8	.8	.7	.0	.1
20.	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.5	.3	.3	.1	.2	.9	.8	.7	.0	.1
25.	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.4	.3	.2	.1	.1	.8	.7	.7	.0	.1
30.	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.3	.2	.2	.1	.1	.8	.7	.7	.0	.1
35.	.0	.0	.0	.0	.1	.2	.1	.1	.1	.0	.2	.2	.2	.1	.1	.8	.7	.7	.0	.1
40.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.0	.1	.4	.2	.1	.1	.7	.7	.7	.0	.1
45.	.0	.0	.0	.0	.2	.2	.0	.1	.1	.0	.2	.4	.2	.1	.1	.7	.8	.8	.0	.1
50.	.0	.0	.0	.0	.2	.2	.0	.1	.0	.0	.2	.3	.2	.1	.1	.7	.8	.8	.0	.1
55.	.0	.0	.0	.0	.2	.2	.0	.1	.0	.0	.2	.3	.2	.1	.1	.7	.8	.8	.0	.1
60.	.0	.0	.0	.0	.2	.2	.0	.1	.0	.0	.2	.3	.1	.1	.1	.7	.8	.9	.0	.1
65.	.0	.0	.0	.0	.2	.2	.0	.1	.0	.0	.2	.3	.1	.1	.1	.7	.9	.9	.0	.1
70.	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.2	.2	.1	.1	.1	.7	.9	.9	.0	.1
75.	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.4	.1	.1	.1	.1	.4	.8	.8	.0	.1
80.	.1	.0	.0	.0	.2	.1	.0	.0	.0	.0	.3	.1	.1	.1	.1	.3	.7	.7	.1	.1
85.	.1	.1	.0	.0	.1	.1	.0	.0	.0	.0	.3	.1	.1	.1	.1	.3	.5	.7	.2	.2
90.	.2	.1	.0	.0	.1	.0	.0	.0	.0	.0	.4	.1	.1	.1	.1	.4	.4	.4	.3	.4
95.	.3	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.2	.2	.3	.5
100.	.3	.2	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.1	.1	.3	.5
105.	.4	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.0	.0	.2	.6
110.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.0	.0	.2	.6
115.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.1	.0	.0	.1	.6
120.	.3	.3	.0	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.1	.0	.0	.1	.6
125.	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.1	.0	.0	.1	.6
130.	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.1	.0	.0	.1	.5
135.	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.1	.0	.0	.1	.5
140.	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.1	.1	.1	.0	.0	.1	.5
145.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.1	.5
150.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.1	.5
155.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.1	.1	.1	.1	.0	.1	.5

160.	*	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.0	.1	.5
165.	*	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.0	.1	.5
170.	*	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.1	.1	.0	.0	.1	.5
175.	*	.2	.2	.2	.0	.2	.0	.0	.1	.1	.1	.2	.2	.2	.1	.1	.1	.0	.0	.1	.5
180.	*	.2	.2	.2	.0	.2	.0	.0	.1	.1	.1	.1	.1	.1	.1	.1	.0	.0	.0	.1	.5
185.	*	.2	.2	.2	.0	.4	.0	.0	.2	.2	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.5
190.	*	.3	.2	.2	.0	.4	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
195.	*	.3	.2	.2	.0	.5	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
200.	*	.3	.3	.2	.0	.5	.1	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
205.	*	.3	.3	.2	.0	.5	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	.3	.3	.2	.0	.5	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
215.	.3	.2	.2	.0	.5	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
220.	.4	.3	.3	.0	.5	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
225.	.5	.3	.3	.0	.5	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
230.	.5	.3	.3	.0	.5	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
235.	.5	.3	.3	.0	.4	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
240.	.5	.3	.3	.0	.4	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
245.	.4	.3	.3	.0	.4	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.4
250.	.4	.5	.4	.0	.3	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.4
255.	.5	.4	.5	.0	.4	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.0	.0	.1	.3
260.	.5	.5	.5	.0	.5	.2	.1	.1	.1	.1	.1	.0	.0	.0	.0	.1	.1	.0	.1	.2
265.	.6	.6	.4	.2	.6	.1	.2	.1	.1	.1	.2	.0	.0	.0	.0	.2	.2	.1	.1	.2
270.	.5	.6	.3	.2	.7	.4	.2	.1	.1	.1	.5	.0	.0	.0	.0	.5	.4	.3	.1	.1
275.	.4	.3	.3	.0	.6	.4	.3	.2	.1	.1	.6	.0	.0	.0	.0	.6	.5	.3	.1	.1
280.	.2	.3	.2	.0	.6	.3	.3	.2	.1	.1	.7	.1	.0	.0	.0	.8	.7	.5	.0	.0
285.	.1	.1	.1	.0	.5	.4	.4	.3	.1	.1	.8	.1	.0	.0	.0	.8	.7	.6	.0	.0
290.	.1	.1	.1	.0	.4	.3	.4	.3	.2	.1	.7	.2	.0	.0	.0	.8	.8	.6	.0	.0
295.	.1	.1	.1	.0	.3	.3	.4	.3	.2	.1	.7	.2	.1	.0	.0	.8	.8	.7	.0	.0
300.	.1	.1	.1	.0	.4	.3	.3	.3	.2	.2	.7	.2	.1	.0	.0	.8	.7	.7	.0	.0
305.	.1	.1	.1	.0	.2	.3	.3	.3	.3	.2	.6	.2	.1	.1	.0	.7	.7	.7	.0	.0
310.	.1	.1	.1	.0	.1	.3	.3	.4	.3	.2	.6	.2	.1	.1	.0	.7	.7	.7	.0	.0
315.	.1	.1	.1	.0	.2	.3	.3	.3	.3	.2	.5	.2	.2	.1	.0	.7	.7	.6	.0	.0
320.	.1	.1	.1	.0	.2	.3	.3	.3	.2	.2	.4	.2	.2	.1	.0	.6	.6	.6	.0	.0
325.	.1	.1	.1	.0	.2	.3	.3	.4	.2	.2	.4	.2	.2	.1	.0	.6	.6	.6	.0	.0
330.	.2	.1	.1	.0	.3	.3	.3	.3	.2	.2	.4	.2	.2	.1	.0	.6	.6	.6	.0	.0
335.	.2	.1	.1	.0	.4	.3	.3	.4	.2	.2	.3	.2	.1	.1	.1	.6	.6	.6	.0	.0
340.	.2	.1	.1	.0	.4	.3	.3	.5	.3	.2	.3	.2	.1	.1	.1	.6	.6	.6	.0	.0
345.	.2	.2	.0	.0	.4	.4	.3	.6	.4	.2	.2	.1	.1	.1	.1	.6	.6	.6	.0	.0
350.	.2	.2	.0	.0	.4	.4	.2	.6	.5	.3	.4	.3	.2	.1	.1	.6	.6	.5	.0	.0
355.	.2	.1	.0	.0	.4	.3	.2	.6	.5	.4	.3	.3	.3	.3	.3	.6	.6	.6	.0	.0
MAX	.6	.6	.5	.2	.7	.4	.4	.6	.5	.4	.8	.4	.5	.4	.3	.9	.9	.9	.3	.6
DEGR.	265	265	255	265	270	270	285	345	350	355	285	0	10	5	0	20	65	60	90	105

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	.0	.2	.4	.5	.4	.4	.4	.3	.3	.3	.3
5.	.1	.2	.5	.5	.5	.5	.4	.2	.2	.2	.2
10.	.2	.2	.5	.5	.6	.4	.5	.0	.1	.1	.1
15.	.2	.3	.5	.5	.4	.3	.5	.0	.0	.0	.0
20.	.2	.2	.5	.5	.3	.2	.5	.0	.0	.0	.0
25.	.1	.2	.4	.4	.3	.2	.4	.0	.0	.0	.0
30.	.1	.2	.4	.4	.3	.2	.3	.0	.0	.0	.0
35.	.1	.2	.3	.5	.3	.2	.3	.0	.0	.0	.0
40.	.1	.2	.3	.5	.3	.2	.3	.0	.0	.0	.0
45.	.1	.2	.3	.4	.3	.2	.3	.0	.0	.0	.0
50.	.1	.2	.3	.3	.2	.1	.3	.0	.0	.0	.0
55.	.1	.1	.3	.3	.1	.1	.3	.0	.0	.0	.0
60.	.1	.1	.2	.3	.1	.1	.3	.0	.0	.0	.0
65.	.1	.1	.2	.2	.1	.1	.3	.0	.0	.0	.0
70.	.1	.1	.2	.2	.1	.1	.3	.0	.0	.0	.0
75.	.1	.1	.2	.1	.1	.1	.3	.0	.0	.0	.0
80.	.1	.1	.2	.1	.1	.1	.3	.0	.0	.0	.0
85.	.2	.2	.3	.1	.1	.1	.3	.0	.0	.0	.0
90.	.3	.2	.3	.1	.1	.1	.3	.0	.0	.0	.0
95.	.4	.2	.4	.1	.1	.1	.3	.0	.0	.0	.0
100.	.4	.3	.4	.1	.1	.1	.3	.0	.0	.0	.0
105.	.4	.3	.3	.1	.1	.1	.3	.0	.0	.0	.0
110.	.5	.2	.3	.1	.1	.1	.3	.0	.0	.0	.0
115.	.5	.4	.3	.1	.1	.1	.3	.0	.0	.0	.1
120.	.6	.6	.1	.1	.1	.1	.3	.0	.0	.0	.1
125.	.6	.6	.1	.1	.1	.1	.3	.0	.0	.0	.1
130.	.5	.7	.3	.1	.1	.1	.3	.0	.0	.1	.1
135.	.5	.6	.4	.2	.2	.2	.3	.0	.0	.1	.1
140.	.5	.6	.3	.2	.2	.2	.3	.0	.0	.1	.1
145.	.6	.6	.3	.2	.2	.2	.3	.0	.0	.1	.1
150.	.6	.6	.3	.2	.2	.2	.3	.0	.1	.1	.1
155.	.6	.6	.3	.2	.2	.2	.4	.0	.1	.1	.1

160.	*	.6	.6	.4	.2	.2	.2	.5	.0	.0	.1	.1
165.	*	.6	.6	.4	.2	.2	.2	.5	.0	.0	.0	.1
170.	*	.5	.6	.3	.3	.3	.2	.5	.0	.0	.0	.1
175.	*	.5	.6	.3	.2	.2	.2	.3	.1	.2	.1	.1
180.	*	.5	.5	.2	.2	.2	.2	.3	.2	.2	.2	.2
185.	*	.5	.5	.3	.1	.1	.1	.2	.3	.3	.2	.2
190.	*	.5	.5	.2	.1	.1	.1	.1	.4	.4	.3	.3
195.	*	.5	.5	.2	.0	.0	.0	.1	.5	.4	.3	.3
200.	*	.5	.5	.3	.0	.0	.0	.1	.5	.5	.5	.2
205.	*	.5	.5	.3	.0	.0	.0	.1	.5	.5	.5	.3

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	.5	.5	.4	.0	.0	.0	.0	.4	.5	.5	.3
215.	.5	.5	.4	.0	.0	.0	.0	.3	.5	.5	.3
220.	.5	.5	.4	.0	.0	.0	.0	.3	.4	.4	.3
225.	.5	.5	.5	.0	.0	.0	.0	.3	.4	.4	.5
230.	.5	.5	.5	.0	.0	.0	.0	.3	.4	.4	.5
235.	.6	.6	.5	.0	.0	.0	.0	.3	.4	.4	.5
240.	.6	.6	.6	.0	.0	.0	.0	.3	.3	.4	.5
245.	.6	.6	.6	.0	.0	.0	.0	.3	.3	.4	.5
250.	.5	.6	.6	.0	.0	.0	.0	.3	.3	.3	.5
255.	.5	.6	.6	.0	.0	.0	.0	.3	.3	.3	.4
260.	.4	.5	.5	.0	.0	.0	.0	.3	.3	.3	.4
265.	.3	.4	.4	.0	.0	.0	.0	.3	.3	.3	.3
270.	.2	.3	.3	.0	.0	.0	.0	.3	.3	.3	.3
275.	.2	.2	.2	.0	.0	.0	.0	.3	.3	.3	.3
280.	.0	.0	.0	.1	.0	.0	.0	.3	.3	.3	.3
285.	.0	.0	.0	.1	.0	.0	.0	.3	.3	.3	.3
290.	.0	.0	.0	.2	.0	.0	.0	.3	.3	.3	.3
295.	.0	.0	.0	.2	.1	.0	.0	.3	.3	.3	.3
300.	.0	.0	.0	.2	.1	.0	.0	.3	.3	.3	.3
305.	.0	.0	.0	.2	.1	.1	.0	.3	.3	.3	.3
310.	.0	.0	.0	.2	.2	.1	.0	.3	.3	.3	.3
315.	.0	.0	.0	.2	.2	.1	.0	.3	.3	.3	.3
320.	.0	.0	.0	.2	.2	.1	.0	.3	.3	.3	.3
325.	.0	.0	.0	.2	.2	.1	.0	.3	.4	.4	.3
330.	.0	.0	.0	.2	.2	.1	.0	.3	.4	.4	.3
335.	.0	.0	.0	.2	.1	.1	.0	.4	.4	.4	.4
340.	.0	.0	.0	.1	.1	.1	.0	.4	.4	.4	.4
345.	.0	.0	.0	.1	.1	.1	.0	.4	.4	.4	.4
350.	.0	.0	.2	.3	.3	.2	.1	.4	.4	.5	.4
355.	.0	.0	.2	.3	.3	.4	.2	.3	.4	.4	.4
MAX	.6	.7	.6	.5	.6	.5	.5	.5	.5	.5	.5
DEGR.	120	130	240	0	10	5	10	195	200	200	225

THE HIGHEST CONCENTRATION OF .90 PPM OCCURRED AT RECEPTOR REC36.

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'LLOYD WINERY PROPERTY CAL3QHC ANAL.21'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'  -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
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'LLOYD WINERY PROP PM 21 BLD, NW SIDE'          8  1  0  'C'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   347  34.82  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  127  34.82  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  1149 34.82  1600 2 3
  1
'LINK4 ROUTE 9W  NFR'  'AG'    0.    0.  0.   1200.   3091.  3.44  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   227.  3.54  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  946. 3.54  0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1661 34.82  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   2304.  3.44  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
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JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:56:16

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 PPM

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-486.8	-12.0	433.	270.	AG	160.	100.0	.0	24.0	1.22	22.0
2. LINK2 MACKS LN WBQ	53.0	6.0	361.7	6.0	309.	90.	AG	82.	100.0	.0	12.0	1.20	15.7
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-114.6	80.	180.	AG	118.	100.0	.0	36.0	.46	4.0
4. LINK4 ROUTE 9W	.0	.0	.0	1200.0	1200.	360.	AG	3091.	3.4	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	227.	3.5	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	946.	3.5	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	9475.9	9431.	360.	AG	44.	100.0	.0	12.0	2.17	479.1
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	2304.	3.4	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:56:16

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. LINK1 CHAPEL HILL E	90	77	3.0	347	1600	34.82	2	3
2. LINK2 MACKS LN WBQ	90	79	3.0	127	1600	34.82	2	3
3. LINK3 ROUTE 9W NBQ	90	38	3.0	1149	1600	34.82	2	3
7. LINK7 ROUTE 9W SBQ	90	42	3.0	1661	1600	34.82	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0
27. RECP BB SIDEWALK	304.0	-22.0	6.0

28.	RECP CC SIDEWALK	*	40.0	-122.0	6.0	*
29.	RECP DD SIDEWALK	*	40.0	-204.0	6.0	*
30.	RECP EE SIDEWALK	*	40.0	-286.0	6.0	*
31.	RECP FF SIDEWALK	*	-40.0	-40.0	6.0	*
32.	RECP GG SIDEWALK	*	-40.0	-122.0	6.0	*
33.	RECP HH SIDEWALK	*	-40.0	-204.0	6.0	*
34.	RECP II SIDEWALK	*	-40.0	-286.0	6.0	*
35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:56:16

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
42. RECP QQ SIDEWALK	-122.0	25.0	6.0
43. RECP RR SIDEWALK	-40.0	30.0	6.0
44. RECP SS SIDEWALK	-22.0	-122.0	6.0
45. RECP TT SIDEWALK	-22.0	-204.0	6.0
46. RECP UU SIDEWALK	-22.0	-286.0	6.0
47. RECP VV SIDEWALK	-42.0	600.0	6.0
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	.0	.3	.2	.1	.3	.3	.6	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.4
5.	.0	.1	.0	.1	.3	.4	.7	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.3
10.	.0	.1	.0	.1	.2	.3	.6	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1
15.	.0	.1	.0	.1	.2	.2	.6	.2	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0
20.	.0	.1	.0	.1	.2	.1	.6	.2	.0	.0	.0	.0	.1	.0	.0	.0	.0	.0	.2	.0
25.	.0	.1	.0	.1	.2	.1	.7	.3	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.3	.0
30.	.0	.1	.0	.1	.1	.1	.7	.3	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
35.	.0	.1	.0	.1	.1	.1	.6	.3	.0	.0	.0	.0	.1	.1	.0	.0	.0	.0	.2	.0
40.	.0	.1	.0	.1	.1	.1	.6	.3	.0	.1	.0	.0	.1	.1	.1	.0	.0	.0	.2	.0
45.	.0	.1	.0	.1	.1	.1	.5	.3	.0	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1	.0
50.	.0	.1	.0	.1	.1	.1	.4	.3	.0	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1	.0
55.	.0	.0	.0	.1	.1	.1	.2	.3	.1	.1	.0	.0	.1	.1	.1	.0	.0	.0	.1	.0
60.	.0	.0	.0	.1	.1	.1	.2	.3	.1	.1	.0	.0	.1	.1	.0	.0	.0	.0	.1	.0
65.	.0	.0	.0	.1	.1	.1	.3	.2	.1	.1	.1	.0	.1	.1	.0	.0	.0	.0	.1	.0
70.	.0	.0	.0	.1	.1	.1	.2	.1	.1	.2	.1	.0	.1	.1	.0	.0	.0	.0	.1	.0
75.	.0	.0	.0	.1	.1	.1	.2	.1	.1	.3	.2	.1	.1	.1	.0	.0	.0	.0	.1	.0
80.	.0	.0	.0	.2	.1	.1	.3	.0	.0	.3	.1	.1	.1	.1	.0	.0	.0	.0	.1	.0
85.	.0	.0	.0	.2	.1	.1	.3	.0	.0	.3	.1	.1	.1	.1	.1	.0	.0	.0	.1	.1
90.	.0	.0	.0	.2	.1	.1	.3	.0	.0	.2	.1	.0	.1	.1	.1	.0	.0	.1	.1	.2
95.	.0	.0	.0	.1	.1	.1	.2	.0	.0	.1	.0	.0	.1	.1	.2	.0	.1	.2	.1	.2
100.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.1	.1	.4	.0	.1	.2	.1	.3
105.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.1	.2	.4	.0	.1	.2	.1	.3
110.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.2	.4	.3	.0	.1	.1	.1	.3
115.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.2	.4	.3	.1	.1	.1	.1	.3
120.	.0	.0	.0	.0	.1	.1	.2	.0	.0	.0	.0	.0	.2	.4	.2	.1	.0	.1	.1	.3
125.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.4	.2	.1	.0	.1	.1	.2
130.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.3	.1	.1	.0	.1	.1	.2
135.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.3	.3	.1	.1	.0	.1	.1	.2
140.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.3	.2	.1	.1	.0	.1	.1	.2
145.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.3	.2	.0	.1	.0	.0	.2	.1
150.	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.3	.2	.0	.0	.0	.0	.1	.1
155.	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.3	.2	.0	.0	.0	.0	.1	.1

160.	*	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.3	.2	.0	.0	.0	.0	.2	.1
165.	*	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.2	.0
170.	*	.0	.0	.0	.0	.1	.2	.1	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.2	.1
175.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.2	.2
180.	*	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.1	.4
185.	*	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.1	.4
190.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.1	.5
195.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.2	.0	.0	.0	.0	.1	.4
200.	*	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.1	.4
205.	*	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.1	.4

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40	
REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51										
210. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.0	.0	.0	.0	.1	.3
215. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.0	.0	.0	.0	.1	.3
220. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.1	.0	.0	.0	.0	.2
225. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.1	.0	.0	.0	.0	.2
230. *	.0	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.0	.1	.0	.0	.0	.0	.2
235. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.4
240. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.5
245. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2	.1	.1	.0	.0	.0	.0	.5
250. *	.2	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.6
255. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.7
260. *	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.1	.1	.1	.0	.0	.0	.0	.7
265. *	.1	.1	.1	.0	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.7
270. *	.1	.1	.1	.0	.0	.0	.3	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.6
275. *	.1	.2	.1	.0	.0	.0	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
280. *	.1	.2	.1	.0	.0	.0	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
285. *	.1	.3	.1	.0	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
290. *	.1	.4	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.2
295. *	.1	.4	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
300. *	.1	.4	.1	.1	.0	.0	.6	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
305. *	.1	.3	.1	.1	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.3
310. *	.1	.3	.1	.1	.0	.0	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
315. *	.1	.3	.1	.1	.0	.1	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
320. *	.1	.3	.2	.1	.0	.1	.5	.0	.0	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
325. *	.1	.2	.2	.1	.0	.1	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
330. *	.1	.1	.2	.1	.1	.1	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
335. *	.0	.2	.2	.1	.1	.1	.5	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.4
340. *	.0	.3	.2	.1	.1	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
345. *	.0	.4	.2	.1	.1	.1	.4	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
350. *	.0	.4	.2	.1	.1	.1	.3	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
355. *	.0	.3	.3	.1	.2	.3	.5	.1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.5
MAX *	.2	.4	.3	.2	.3	.4	.7	.3	.1	.3	.2	.1	.3	.4	.4	.1	.1	.2	.3	.7
DEGR. *	240	290	355	80	0	5	5	25	55	75	75	75	135	110	100	115	95	95	25	255

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	.2	.0	.0	.0	.4	.2	.2	.6	.4	.5	.6	.5	.4	.4	.3	.8	.6	.6	.0	.0
5.	.0	.0	.0	.0	.3	.2	.2	.4	.3	.3	.7	.4	.4	.5	.4	.8	.8	.7	.0	.1
10.	.0	.0	.0	.0	.1	.2	.2	.3	.1	.1	.7	.5	.5	.6	.3	.8	.8	.7	.0	.1
15.	.0	.0	.0	.0	.1	.2	.2	.1	.1	.0	.6	.5	.5	.4	.2	.8	.8	.7	.0	.1
20.	.0	.0	.0	.0	.1	.2	.2	.1	.1	.0	.6	.4	.4	.3	.2	.9	.8	.7	.0	.1
25.	.0	.0	.0	.0	.1	.2	.2	.1	.1	.1	.4	.3	.3	.3	.2	.9	.7	.7	.0	.1
30.	.0	.0	.0	.0	.1	.2	.2	.1	.1	.1	.4	.4	.3	.2	.2	.9	.7	.7	.0	.1
35.	.0	.0	.0	.0	.1	.2	.2	.1	.1	.0	.3	.4	.4	.2	.2	.9	.7	.7	.1	.1
40.	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.3	.5	.4	.3	.2	.8	.7	.7	.1	.1
45.	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.2	.5	.3	.2	.2	.7	.8	.8	.1	.1
50.	.0	.0	.0	.0	.2	.2	.2	.1	.1	.0	.2	.5	.3	.2	.2	.7	.8	.8	.1	.1
55.	.0	.0	.0	.0	.2	.2	.2	.1	.0	.0	.2	.5	.3	.2	.1	.7	.8	.8	.1	.1
60.	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.2	.4	.1	.1	.1	.7	.8	.9	.1	.1
65.	.0	.0	.0	.0	.2	.2	.1	.1	.0	.0	.2	.4	.1	.1	.1	.7	.9	.9	.1	.1
70.	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.2	.4	.1	.1	.1	.7	.8	.9	.0	.1
75.	.0	.0	.0	.0	.2	.2	.1	.0	.0	.0	.4	.3	.1	.1	.1	.5	.9	.9	.0	.1
80.	.1	.1	.0	.0	.2	.1	.0	.0	.0	.0	.4	.2	.1	.1	.1	.4	.7	.8	.1	.1
85.	.1	.1	.0	.0	.1	.1	.0	.0	.0	.0	.3	.2	.1	.1	.1	.4	.5	.7	.3	.2
90.	.2	.2	.1	.0	.1	.1	.0	.0	.0	.0	.4	.2	.1	.1	.1	.4	.5	.5	.4	.5
95.	.3	.2	.1	.0	.1	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.4	.2	.5	.5
100.	.3	.3	.1	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.3	.1	.5	.5
105.	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.2	.0	.4	.6
110.	.4	.3	.2	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.2	.0	.3	.6
115.	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.1	.1	.2	.6
120.	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.3	.1	.1	.1	.1	.2	.1	.1	.2	.7
125.	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.4	.2	.2	.2	.1	.1	.1	.1	.1	.7
130.	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.4	.2	.2	.2	.2	.1	.1	.1	.1	.6
135.	.3	.3	.3	.0	.0	.0	.0	.0	.0	.0	.4	.2	.2	.2	.2	.1	.1	.1	.1	.6
140.	.3	.3	.2	.0	.0	.0	.0	.0	.0	.0	.4	.2	.2	.2	.2	.1	.1	.1	.1	.6
145.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.2	.2	.1	.1	.1	.1	.6
150.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.2	.2	.1	.1	.1	.1	.6
155.	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.3	.2	.2	.2	.2	.1	.1	.1	.1	.6

160.	*	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.1	.1	.6
165.	*	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.2	.2	.2	.2	.2	.1	.1	.0	.1	.5
170.	*	.2	.2	.2	.0	.1	.0	.0	.0	.0	.0	.3	.2	.2	.2	.2	.1	.1	.0	.1	.5
175.	*	.2	.2	.2	.0	.2	.0	.0	.1	.1	.1	.2	.2	.2	.2	.2	.1	.0	.0	.1	.5
180.	*	.2	.2	.2	.0	.4	.0	.0	.2	.2	.2	.2	.2	.2	.2	.1	.0	.0	.0	.1	.5
185.	*	.3	.2	.2	.0	.5	.0	.0	.2	.2	.2	.1	.1	.1	.1	.1	.0	.0	.0	.1	.5
190.	*	.3	.3	.2	.0	.7	.0	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
195.	*	.3	.3	.2	.0	.6	.1	.0	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
200.	*	.3	.3	.3	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
205.	*	.3	.3	.3	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	.3	.3	.3	.0	.7	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
215.	.4	.3	.3	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
220.	.5	.4	.4	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
225.	.5	.4	.4	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
230.	.5	.4	.4	.0	.6	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.5
235.	.5	.5	.3	.0	.5	.1	.1	.2	.2	.2	.0	.0	.0	.0	.0	.0	.0	.0	.1	.6
240.	.5	.5	.3	.0	.4	.1	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.6
245.	.6	.5	.3	.0	.4	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.6
250.	.6	.6	.4	.0	.3	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.0	.0	.0	.1	.6
255.	.6	.5	.5	.0	.4	.2	.0	.1	.1	.1	.0	.0	.0	.0	.0	.1	.1	.0	.1	.5
260.	.7	.5	.5	.2	.5	.3	.2	.1	.1	.1	.1	.0	.0	.0	.0	.2	.1	.1	.1	.4
265.	.7	.6	.6	.2	.6	.3	.2	.1	.1	.1	.3	.0	.0	.0	.0	.3	.3	.2	.1	.3
270.	.5	.6	.4	.2	.7	.4	.4	.1	.1	.1	.5	.0	.0	.0	.0	.6	.5	.4	.1	.2
275.	.5	.3	.4	.2	.7	.4	.4	.3	.1	.1	.7	.1	.0	.0	.0	.7	.7	.6	.1	.2
280.	.2	.3	.3	.0	.6	.4	.4	.3	.1	.1	.8	.1	.0	.0	.0	.8	.8	.7	.0	.0
285.	.1	.1	.1	.0	.5	.4	.5	.6	.2	.1	.8	.3	.0	.0	.0	.9	.8	.8	.0	.0
290.	.1	.1	.1	.0	.4	.3	.4	.6	.2	.1	.8	.2	.1	.0	.0	.8	.8	.8	.0	.0
295.	.1	.1	.1	.1	.3	.3	.4	.6	.2	.2	.7	.3	.1	.0	.0	.8	.8	.8	.0	.0
300.	.1	.1	.1	.1	.4	.3	.3	.6	.3	.2	.7	.3	.1	.1	.0	.8	.8	.7	.0	.0
305.	.1	.1	.1	.1	.3	.3	.3	.7	.4	.3	.6	.2	.2	.1	.0	.7	.7	.7	.0	.0
310.	.1	.1	.1	.1	.2	.3	.3	.7	.4	.3	.6	.2	.2	.1	.0	.7	.7	.7	.0	.0
315.	.1	.1	.1	.1	.2	.3	.3	.8	.4	.3	.5	.2	.2	.1	.0	.7	.7	.7	.0	.0
320.	.1	.1	.1	.1	.2	.3	.3	.7	.3	.3	.4	.2	.2	.1	.0	.6	.6	.6	.0	.0
325.	.1	.1	.1	.1	.3	.3	.3	.7	.3	.3	.4	.2	.2	.1	.0	.6	.6	.6	.0	.0
330.	.3	.1	.1	.0	.4	.3	.3	.7	.4	.3	.4	.2	.2	.1	.1	.6	.6	.6	.0	.0
335.	.3	.1	.1	.0	.4	.3	.3	.6	.4	.3	.3	.2	.1	.1	.1	.6	.6	.6	.0	.0
340.	.3	.1	.1	.0	.5	.3	.3	.8	.4	.3	.3	.2	.1	.1	.1	.6	.6	.6	.0	.0
345.	.3	.2	.1	.0	.5	.4	.3	.9	.7	.4	.2	.1	.1	.1	.1	.6	.6	.6	.0	.0
350.	.2	.2	.0	.0	.5	.4	.2	.9	.6	.6	.4	.3	.2	.2	.1	.6	.6	.6	.0	.0
355.	.2	.1	.0	.0	.5	.3	.2	.7	.6	.5	.4	.4	.3	.3	.4	.6	.6	.6	.0	.0
MAX	.7	.6	.6	.2	.7	.4	.5	.9	.7	.6	.8	.5	.5	.6	.4	.9	.9	.9	.5	.7
DEGR.	260	250	265	260	190	270	285	345	345	350	280	0	10	10	5	20	75	60	95	120

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	.0	.2	.5	.5	.5	.6	.4	.3	.4	.4	.3
5.	.2	.2	.6	.6	.6	.6	.5	.2	.3	.3	.2
10.	.2	.3	.6	.7	.6	.6	.5	.0	.1	.1	.1
15.	.2	.3	.6	.5	.6	.5	.6	.0	.0	.0	.0
20.	.2	.3	.6	.5	.6	.4	.6	.0	.0	.0	.0
25.	.1	.3	.4	.6	.4	.3	.4	.0	.0	.0	.0
30.	.1	.3	.4	.6	.5	.3	.4	.0	.0	.0	.0
35.	.1	.3	.4	.6	.4	.2	.4	.0	.0	.0	.0
40.	.1	.3	.4	.6	.3	.2	.4	.0	.0	.0	.0
45.	.1	.2	.4	.6	.3	.2	.4	.0	.0	.0	.0
50.	.1	.2	.4	.6	.3	.2	.3	.0	.0	.0	.0
55.	.1	.1	.3	.6	.3	.2	.3	.0	.0	.0	.0
60.	.1	.1	.2	.6	.2	.2	.3	.0	.0	.0	.0
65.	.1	.1	.2	.5	.2	.2	.3	.0	.0	.0	.0
70.	.1	.1	.2	.5	.2	.2	.3	.0	.0	.0	.0
75.	.1	.1	.2	.4	.2	.2	.3	.0	.0	.0	.0
80.	.1	.1	.3	.3	.2	.2	.3	.0	.0	.0	.0
85.	.2	.2	.3	.3	.2	.2	.3	.0	.0	.0	.0
90.	.3	.2	.3	.3	.2	.2	.3	.0	.0	.0	.0
95.	.5	.2	.4	.2	.2	.2	.3	.0	.0	.0	.0
100.	.4	.3	.4	.2	.2	.2	.3	.0	.0	.0	.0
105.	.4	.3	.3	.2	.2	.2	.3	.0	.0	.0	.0
110.	.7	.4	.3	.2	.2	.2	.3	.0	.0	.0	.1
115.	.7	.5	.3	.2	.2	.2	.3	.0	.0	.0	.1
120.	.8	.6	.2	.2	.2	.2	.3	.0	.0	.0	.1
125.	.7	.6	.2	.2	.2	.2	.3	.0	.0	.1	.1
130.	.6	.7	.3	.2	.2	.2	.3	.0	.0	.1	.1
135.	.6	.7	.4	.2	.2	.2	.4	.0	.0	.1	.1
140.	.6	.7	.4	.2	.2	.2	.4	.0	.0	.1	.1
145.	.6	.6	.5	.2	.2	.2	.4	.0	.1	.1	.1
150.	.6	.6	.5	.3	.3	.3	.4	.0	.1	.1	.1
155.	.6	.6	.5	.3	.3	.3	.4	.0	.1	.1	.1

160.	*	.6	.6	.4	.3	.3	.3	.6	.0	.0	.1	.1
165.	*	.6	.6	.4	.3	.3	.3	.6	.0	.0	.0	.1
170.	*	.6	.6	.5	.4	.4	.4	.5	.0	.0	.0	.1
175.	*	.5	.6	.3	.3	.3	.3	.5	.1	.2	.2	.2
180.	*	.5	.5	.3	.3	.3	.3	.4	.3	.2	.3	.3
185.	*	.5	.5	.3	.2	.2	.2	.2	.5	.3	.5	.3
190.	*	.5	.5	.2	.1	.1	.1	.1	.4	.5	.4	.4
195.	*	.5	.5	.2	.0	.0	.0	.1	.6	.5	.4	.4
200.	*	.5	.5	.3	.0	.0	.0	.1	.6	.6	.5	.4
205.	*	.5	.5	.3	.0	.0	.0	.1	.5	.6	.5	.3

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	.5	.5	.4	.0	.0	.0	.1	.5	.5	.5	.3
215.	.5	.5	.4	.0	.0	.0	.0	.5	.5	.5	.3
220.	.5	.5	.4	.0	.0	.0	.0	.4	.5	.5	.4
225.	.5	.5	.5	.0	.0	.0	.0	.4	.5	.6	.5
230.	.5	.5	.5	.0	.0	.0	.0	.3	.5	.6	.5
235.	.6	.6	.5	.0	.0	.0	.0	.3	.5	.6	.5
240.	.6	.6	.6	.0	.0	.0	.0	.3	.5	.5	.5
245.	.6	.6	.6	.0	.0	.0	.0	.3	.4	.5	.5
250.	.6	.6	.6	.0	.0	.0	.0	.3	.4	.5	.6
255.	.6	.6	.6	.0	.0	.0	.0	.3	.4	.4	.6
260.	.5	.6	.6	.0	.0	.0	.0	.3	.4	.4	.4
265.	.4	.5	.5	.0	.0	.0	.0	.3	.3	.3	.4
270.	.3	.4	.3	.0	.0	.0	.0	.3	.3	.3	.3
275.	.2	.2	.2	.1	.0	.0	.0	.3	.3	.3	.3
280.	.0	.1	.1	.1	.0	.0	.0	.3	.4	.4	.3
285.	.0	.0	.0	.3	.0	.0	.0	.3	.4	.4	.3
290.	.0	.0	.0	.2	.1	.0	.0	.3	.4	.4	.3
295.	.0	.0	.0	.3	.1	.0	.0	.3	.4	.4	.3
300.	.0	.0	.0	.3	.2	.1	.0	.3	.4	.4	.3
305.	.0	.0	.0	.2	.2	.1	.0	.3	.4	.4	.3
310.	.0	.0	.0	.2	.2	.1	.0	.3	.4	.4	.3
315.	.0	.0	.0	.2	.2	.1	.0	.4	.4	.4	.4
320.	.0	.0	.0	.2	.2	.1	.0	.4	.4	.4	.4
325.	.0	.0	.0	.2	.2	.1	.0	.4	.4	.4	.4
330.	.0	.0	.0	.2	.2	.1	.0	.4	.4	.4	.4
335.	.0	.0	.0	.2	.1	.1	.0	.4	.5	.5	.4
340.	.0	.0	.0	.1	.1	.1	.0	.5	.5	.5	.4
345.	.0	.0	.0	.2	.1	.1	.0	.5	.5	.5	.5
350.	.0	.0	.2	.3	.3	.3	.1	.4	.5	.5	.5
355.	.0	.0	.3	.3	.4	.4	.2	.4	.5	.5	.4
MAX	.8	.7	.6	.7	.6	.6	.6	.6	.6	.6	.6
DEGR.	120	130	5	10	5	0	15	195	200	225	250

THE HIGHEST CONCENTRATION OF .90 PPM OCCURRED AT RECEPTOR REC37.

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'LLOYD WINERY PROPERTY CAL3QHC ANAL.11'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'   -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
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'LLOYD WINERY PROP PM 11 EX COND, NW SIDE'          8  1  0  'P'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   309  0.0198  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  117  0.0198  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  656 0.0198  1600 2 3
  1
'LINK4 ROUTE 9W  NFR'  'AG'    0.    0.  0.   1200.   2339.  0.0154  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   205.  0.0154  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  840. 0.0154 0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1369 0.0198  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   1518.  0.0154  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
```

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:56:44

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-285.8	-12.0	232.	270.	AG	0.	100.0	.0	24.0	1.08	11.8
2. LINK2 MACKS LN WBQ	53.0	6.0	255.3	6.0	202.	90.	AG	0.	100.0	.0	12.0	1.10	10.3
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-80.3	45.	180.	AG	0.	100.0	.0	36.0	.26	2.3
4. LINK4 ROUTE 9W	.0	.0	.0	1200.0	1200.	360.	AG	2339.	.0	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	205.	.0	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	840.	.0	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	6496.0	6451.	360.	AG	0.	100.0	.0	12.0	1.79	327.7
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	1518.	.0	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:56:44

1. LINK1 CHAPEL HILL	E*	90	77	3.0	309	1600	.02	2	3
2. LINK2 MACKS LN WBQ	*	90	79	3.0	117	1600	.02	2	3
3. LINK3 ROUTE 9W NBQ	*	90	38	3.0	656	1600	.02	2	3
7. LINK7 ROUTE 9W SBQ	*	90	42	3.0	1369	1600	.02	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0
27. RECP BB SIDEWALK	304.0	-22.0	6.0
28. RECP CC SIDEWALK	40.0	-122.0	6.0
29. RECP DD SIDEWALK	40.0	-204.0	6.0
30. RECP EE SIDEWALK	40.0	-286.0	6.0
31. RECP FF SIDEWALK	-40.0	-40.0	6.0
32. RECP GG SIDEWALK	-40.0	-122.0	6.0
33. RECP HH SIDEWALK	-40.0	-204.0	6.0
34. RECP II SIDEWALK	-40.0	-286.0	6.0

35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*
42.	RECP QQ SIDEWALK	*	-122.0	25.0	6.0	*
43.	RECP RR SIDEWALK	*	-40.0	30.0	6.0	*
44.	RECP SS SIDEWALK	*	-22.0	-122.0	6.0	*
45.	RECP TT SIDEWALK	*	-22.0	-204.0	6.0	*
46.	RECP UU SIDEWALK	*	-22.0	-286.0	6.0	*
47.	RECP VV SIDEWALK	*	-42.0	600.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

DATE : 1/22/13
TIME : 12:56:44

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
5.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
10.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
15.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
20.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
25.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
30.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
35.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
40.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
45.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
50.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
55.	0.	0.	0.	1.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
60.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
65.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
70.	0.	0.	0.	1.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
75.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
85.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
105.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
115.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
125.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
135.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
145.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
150.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
155.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.

160.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
165.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
170.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
175.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
180.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
185.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
190.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
195.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
200.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
205.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND * CONCENTRATION
ANGLE * (ug/m**3)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
215. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
220. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
225. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
230. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
235. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
240. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
245. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
250. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
255. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
260. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
265. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
270. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
275. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
280. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
285. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
290. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
295. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
300. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
305. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
310. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
315. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
320. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
325. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
330. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
335. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
340. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
345. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
350. *	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
355. *	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
MAX *	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	1.	2.
DEGR. *	235	345	350	55	5	5	15	30	40	55	35	50	125	100	100	120	105	95	20	260

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	0.	0.	0.
5.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	1.	1.	1.	0.	0.
15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
25.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
35.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
55.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
60.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
65.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
70.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.
75.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.
80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
85.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
90.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	1.	1.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
105.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.
115.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
125.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
135.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
145.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
155.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.

160.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
165.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
170.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
175.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
180.	*	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
185.	*	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
195.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	*	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
205.	*	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
215.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
225.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
235.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
240.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
245.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
250.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
255.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
260.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
265.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
270.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.
275.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
280.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
285.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
290.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
295.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
300.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
305.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
310.	1.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
315.	1.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
320.	1.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
325.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
330.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
335.	1.	1.	0.	0.	2.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
340.	1.	1.	0.	0.	2.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
345.	1.	0.	0.	0.	2.	1.	0.	2.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
350.	1.	0.	0.	0.	2.	1.	0.	2.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.
355.	0.	0.	0.	0.	2.	0.	0.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
MAX	1.	1.	1.	1.	2.	1.	1.	2.	2.	1.	2.	2.	2.	1.	1.	1.	1.	1.	1.	1.
DEGR.	270	265	260	265	345	275	275	345	355	355	10	10	5	5	5	10	55	70	95	110

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	0.	0.	1.	2.	2.	2.	1.	1.	1.	1.	1.
5.	0.	1.	2.	2.	2.	2.	1.	0.	1.	1.	1.
10.	0.	1.	2.	2.	2.	1.	1.	0.	0.	0.	0.
15.	0.	1.	2.	2.	2.	1.	2.	0.	0.	0.	0.
20.	1.	1.	2.	1.	1.	1.	2.	0.	0.	0.	0.
25.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
30.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
35.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
40.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
45.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
50.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
55.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
60.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
65.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
70.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
75.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
80.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
85.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
90.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
95.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
100.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
105.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
110.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
115.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
120.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
125.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
130.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
135.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
140.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
145.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
150.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
155.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.

160.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
165.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
170.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
175.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.
180.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
185.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
190.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.	1.
195.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.	1.
200.	*	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.
205.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.11 RUN: LLOYD WINERY PROP PM 11 EX COND, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	1.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.
215.	1.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.
220.	1.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.
225.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
230.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
235.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
240.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
245.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
250.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
255.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
260.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
265.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
270.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
275.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
280.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
285.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
290.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
295.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
300.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
305.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
310.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
315.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
320.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
325.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
330.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
335.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.
340.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
345.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.
350.	0.	0.	0.	1.	1.	1.	0.	1.	2.	2.	2.
355.	0.	0.	1.	1.	1.	1.	1.	1.	2.	2.	1.
MAX	1.	1.	2.	2.	2.	2.	2.	2.	2.	2.	2.
DEGR.	110	100	10	5	5	0	165	195	345	345	345

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC44.

```
'LLOYD WINERY PROPERTY CAL3QHC ANAL.21'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'  -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
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'LLOYD WINERY PROP PM 21 NO BLD, NW SIDE'          8  1  0  'P'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   327  0.0169  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  123  0.0169  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  709 0.0169  1600 2 3
  1
'LINK4 ROUTE 9W  NFR'  'AG'    0.    0.  0.   1200.   2480.  0.0120  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   216.  0.0120  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  890. 0.0120  0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1447 0.0169  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   1626.  0.0120  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
```

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57: 9

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-381.0	-12.0	327.	270.	AG	0.	100.0	.0	24.0	1.15	16.6
2. LINK2 MACKS LN WBQ	53.0	6.0	319.2	6.0	266.	90.	AG	0.	100.0	.0	12.0	1.16	13.5
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-84.0	49.	180.	AG	0.	100.0	.0	36.0	.28	2.5
4. LINK4 ROUTE 9W	.0	.0	.0	1200.0	1200.	360.	AG	2480.	.0	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	216.	.0	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	890.	.0	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	7292.0	7247.	360.	AG	0.	100.0	.0	12.0	1.89	368.1
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	1626.	.0	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57: 9

1. LINK1 CHAPEL HILL	E*	90	77	3.0	327	1600	.02	2	3
2. LINK2 MACKS LN WBQ	*	90	79	3.0	123	1600	.02	2	3
3. LINK3 ROUTE 9W NBQ	*	90	38	3.0	709	1600	.02	2	3
7. LINK7 ROUTE 9W SBQ	*	90	42	3.0	1447	1600	.02	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0
27. RECP BB SIDEWALK	304.0	-22.0	6.0
28. RECP CC SIDEWALK	40.0	-122.0	6.0
29. RECP DD SIDEWALK	40.0	-204.0	6.0
30. RECP EE SIDEWALK	40.0	-286.0	6.0
31. RECP FF SIDEWALK	-40.0	-40.0	6.0
32. RECP GG SIDEWALK	-40.0	-122.0	6.0
33. RECP HH SIDEWALK	-40.0	-204.0	6.0

34.	RECP II SIDEWALK	*	-40.0	-286.0	6.0	*
35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*
42.	RECP QQ SIDEWALK	*	-122.0	25.0	6.0	*
43.	RECP RR SIDEWALK	*	-40.0	30.0	6.0	*
44.	RECP SS SIDEWALK	*	-22.0	-122.0	6.0	*
45.	RECP TT SIDEWALK	*	-22.0	-204.0	6.0	*
46.	RECP UU SIDEWALK	*	-22.0	-286.0	6.0	*
47.	RECP VV SIDEWALK	*	-42.0	600.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57: 9

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
5.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
10.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
15.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
25.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
30.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
35.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
40.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
45.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
55.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
65.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
75.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
85.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
105.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	1.	0.	0.	0.	0.	0.
115.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.
125.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
135.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
145.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
155.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.

160.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
165.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
170.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
175.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
180.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
185.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
190.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
195.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
200.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
205.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND * CONCENTRATION
ANGLE * (ug/m**3)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
215. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
220. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
225. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
230. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
235. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
240. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
245. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
250. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
255. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
260. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
265. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
270. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
275. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
280. *	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
285. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
290. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
295. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
300. *	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
305. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
310. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
315. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
320. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
325. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
330. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
335. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
340. *	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
345. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
350. *	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
355. *	0.	0.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
MAX *	0.	1.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.
DEGR. *	240	310	345	60	5	10	10	35	30	45	50	65	110	105	105	120	95	100	20	260

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
5.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
25.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
35.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.
50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.
55.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.
60.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.
65.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
70.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.
75.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.
80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
85.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
90.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
105.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
115.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
125.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
135.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
145.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
155.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
160.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.

165.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
170.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
175.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
180.	*	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.
185.	*	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
190.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
195.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
200.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
205.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
215.	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
220.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
225.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
230.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
235.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
240.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
245.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
250.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
255.	1.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
260.	1.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
265.	1.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
270.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.
275.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
280.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
285.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
290.	0.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
295.	0.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
300.	0.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
305.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
310.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
315.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
320.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
325.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
330.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
335.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
340.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
345.	1.	0.	0.	0.	2.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
350.	1.	0.	0.	0.	2.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
355.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.
MAX	1.	1.	1.	0.	2.	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.
DEGR.	260	260	265	260	345	280	270	350	355	355	10	10	5	0	5	20	35	60	95	100

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.
5.	0.	1.	1.	2.	1.	1.	1.	0.	1.	1.	1.
10.	0.	1.	1.	2.	1.	1.	1.	0.	0.	0.	0.
15.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
20.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
25.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
30.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
35.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
40.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
45.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
50.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
55.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
60.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
65.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
70.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
75.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
80.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.
85.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
90.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
95.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
100.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
105.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
110.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
115.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
120.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
125.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
130.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
135.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
140.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
145.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
150.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
155.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.

160.	*	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
165.	*	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
170.	*	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
175.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.
180.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
185.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
190.	*	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
195.	*	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
200.	*	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
205.	*	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 NO BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
215.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
220.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
225.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
230.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
235.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
240.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
245.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
250.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
255.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
260.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
265.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
270.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
275.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
280.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
285.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
290.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
295.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
300.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
305.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
310.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
315.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
320.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
325.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
330.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
335.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
340.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
345.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.
350.	0.	0.	0.	1.	1.	1.	0.	1.	2.	2.	1.
355.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.
MAX	1.	1.	1.	2.	1.	1.	1.	1.	2.	2.	1.
DEGR.	120	95	10	5	5	5	165	195	345	345	345

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC44.

```
'LLOYD WINERY PROPERTY CAL3QHC ANAL.21'     60. 175.  0. 0. 51   0.3048 1 1
'RECP A  WYNGATE'          399.      308.      6.
'RECP B  RITE AID'         120.     -155.      6.
'RECP C  GOSPEL CHURCH'    102.     -620.      6.
'RECP D  FOX POOLS'       -1011.     -50.      6.
'RECP E  HOUSE 109'        -68.     -640.      6.
'RECP F  WAGON WHEELS'     -69.     -400.      6.
'RECP G  MCCLEAN MOTORS'   -99.      -54.      6.
'RECP H  HOSANNA CHURCH'  -473.     -172.      6.
'RECP I  HOUSE'           -900.     -308.      6.
'RECP J  HOUSE'           -752.      -65.      6.
'RECP K  HOUSE'          -1030.     -106.      6.
'RECP L  HOUSE'          -1183.     -152.      6.
'RECP M  HOUSE 117'       -337.       90.      6.
'RECP N  HOUSE 119'       -445.       80.      6.
'RECP O  HOUSE 121'       -645.       65.      6.
'RECP P  HOUSE'           -718.      335.      6.
'RECP Q  HOUSE'           -983.      166.      6.
'RECP R  HOUSE'          -1088.       65.      6.
'RECP S  PODIATRIST'      -144.      426.      6.
'RECP T  SIDEWALK'          40.       30.      6.
'RECP U  SIDEWALK'         140.       22.      6.
'RECP V  SIDEWALK'         222.       22.      6.
'RECP W  SIDEWALK'         304.       22.      6.
'RECP X  SIDEWALK'         600.       22.      6.
'RECP Y  SIDEWALK'          40.      -30.      6.
'RECP Z  SIDEWALK          140.      -22.      6.
'RECP AA SIDEWALK'         222.      -22.      6.
'RECP BB SIDEWALK'         304.      -22.      6.
'RECP CC SIDEWALK'          40.     -122.      6.
'RECP DD SIDEWALK'          40.     -204.      6.
'RECP EE SIDEWALK'          40.     -286.      6.
'RECP FF SIDEWALK'         -40.      -40.      6.
'RECP GG SIDEWALK'         -40.     -122.      6.
'RECP HH SIDEWALK'         -40.     -204.      6.
'RECP II SIDEWALK'         -40.     -286.      6.
'RECP JJ SIDEWALK'         -42.     -600.      6.
'RECP KK SIDEWALK'        -122.      -35.      6.
'RECP LL SIDEWALK'        -204.      -35.      6.
'RECP MM SIDEWALK'        -286.      -35.      6.
'RECP NN SIDEWALK'        -600.       22.      6.
'RECP OO SIDEWALK'        -286.       25.      6.
'RECP PP SIDEWALK'        -204.       25.      6.
'RECP QQ SIDEWALK'        -122.       25.      6.
'RECP RR SIDEWALK'         -40.       30.      6.
'RECP SS SIDEWALK'         -22.     -122.      6.
'RECP TT SIDEWALK'         -22.     -204.      6.
'RECP UU SIDEWALK'         -22.     -286.      6.
'RECP VV SIDEWALK'         -42.      600.      6.
'RECP WW SIDEWALK'          42.      600.      6.
'RECP XX SIDEWALK'          35.      286.      6.
'RECP YY SIDEWALK'          35.      204.      6.
'RECP ZZ SIDEWALK'          45.      122.      6.
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'LLOYD WINERY PROP PM 21 BLD, NW SIDE'          8  1  0  'P'
  2
'LINK1 CHAPEL HILL  EBQ'  'AG'    -54.   -12.  -154.  -12.    0.  24.0   2
      90        77       3.0   347  0.0169  1600 2 3
  2
'LINK2 MACKS LN WBQ'   'AG'     53.   6.   153.   6.    0.  12.0   1
      90        79       3.0  127  0.0169  1600 2 3
  2
'LINK3 ROUTE 9W NBQ'   'AG'     18.   -35.   18.   -135.    0.  36.0   3
      90        38       3.0  1149 0.0169  1600 2 3
  1
'LINK4 ROUTE 9W  NFR'  'AG'    0.    0.  0.   1200.   3091.  0.0120  0. 24.
  1
'LINK5 MACKS  EFR'  'AG'     0.   0.  1200.    0.   227.  0.0120  0. 24.
  1
'LINK6 CHAPEL HILL WFR'  'AG'    0.    0.  -1200.   0.  946. 0.0120  0. 12.
  2
'LINK7 ROUTE 9W SBQ'  'AG'     -16.  45.    -16.  145.   0.  12.0   1
       90        42       3.0  1661 0.0169  1600 2 3
  1
'LINK8 ROUTE 9W SFR'  'AG'    0.    0.  0.   -1200.   2304.  0.0120  0. 12.
1.0 00. 5  1000. 0.  'Y' 5  0 71
```

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57:45

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S VD = .0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 5 (E) ATIM = 60. MINUTES MIXH = 1000. M AMB = .0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	LINK COORDINATES (FT) X1	Y1	X2	Y2	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. LINK1 CHAPEL HILL E	-54.0	-12.0	-486.8	-12.0	433.	270.	AG	0.	100.0	.0	24.0	1.22	22.0
2. LINK2 MACKS LN WBQ	53.0	6.0	361.7	6.0	309.	90.	AG	0.	100.0	.0	12.0	1.20	15.7
3. LINK3 ROUTE 9W NBQ	18.0	-35.0	18.0	-114.6	80.	180.	AG	0.	100.0	.0	36.0	.46	4.0
4. LINK4 ROUTE 9W NFR	.0	.0	.0	1200.0	1200.	360.	AG	3091.	.0	.0	24.0		
5. LINK5 MACKS EFR	.0	.0	1200.0	.0	1200.	90.	AG	227.	.0	.0	24.0		
6. LINK6 CHAPEL HILL WF	.0	.0	-1200.0	.0	1200.	270.	AG	946.	.0	.0	12.0		
7. LINK7 ROUTE 9W SBQ	-16.0	45.0	-16.0	9475.9	9431.	360.	AG	0.	100.0	.0	12.0	2.17	479.1
8. LINK8 ROUTE 9W SFR	.0	.0	.0	-1200.0	1200.	180.	AG	2304.	.0	.0	12.0		

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57:45

1. LINK1 CHAPEL HILL	E*	90	77	3.0	347	1600	.02	2	3
2. LINK2 MACKS LN WBQ	*	90	79	3.0	127	1600	.02	2	3
3. LINK3 ROUTE 9W NBQ	*	90	38	3.0	1149	1600	.02	2	3
7. LINK7 ROUTE 9W SBQ	*	90	42	3.0	1661	1600	.02	2	3

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
1. RECP A WYNGATE	399.0	308.0	6.0
2. RECP B RITE AID	120.0	-155.0	6.0
3. RECP C GOSPEL CHURC	102.0	-620.0	6.0
4. RECP D FOX POOLS	-1011.0	-50.0	6.0
5. RECP E HOUSE 109	-68.0	-640.0	6.0
6. RECP F WAGON WHEELS	-69.0	-400.0	6.0
7. RECP G MCCLEAN MOTO	-99.0	-54.0	6.0
8. RECP H HOSANNA CHUR	-473.0	-172.0	6.0
9. RECP I HOUSE	-900.0	-308.0	6.0
10. RECP J HOUSE	-752.0	-65.0	6.0
11. RECP K HOUSE	-1030.0	-106.0	6.0
12. RECP L HOUSE	-1183.0	-152.0	6.0
13. RECP M HOUSE 117	-337.0	90.0	6.0
14. RECP N HOUSE 119	-445.0	80.0	6.0
15. RECP O HOUSE 121	-645.0	65.0	6.0
16. RECP P HOUSE	-718.0	335.0	6.0
17. RECP Q HOUSE	-983.0	166.0	6.0
18. RECP R HOUSE	-1088.0	65.0	6.0
19. RECP S PODIATRIST	-144.0	426.0	6.0
20. RECP T SIDEWALK	40.0	30.0	6.0
21. RECP U SIDEWALK	140.0	22.0	6.0
22. RECP V SIDEWALK	222.0	22.0	6.0
23. RECP W SIDEWALK	304.0	22.0	6.0
24. RECP X SIDEWALK	600.0	22.0	6.0
25. RECP Y SIDEWALK	40.0	-30.0	6.0
26. RECP Z SIDEWALK	222.0	-22.0	6.0
27. RECP BB SIDEWALK	304.0	-22.0	6.0
28. RECP CC SIDEWALK	40.0	-122.0	6.0
29. RECP DD SIDEWALK	40.0	-204.0	6.0
30. RECP EE SIDEWALK	40.0	-286.0	6.0
31. RECP FF SIDEWALK	-40.0	-40.0	6.0
32. RECP GG SIDEWALK	-40.0	-122.0	6.0
33. RECP HH SIDEWALK	-40.0	-204.0	6.0
34. RECP II SIDEWALK	-40.0	-286.0	6.0

35.	RECP JJ SIDEWALK	*	-42.0	-600.0	6.0	*
36.	RECP KK SIDEWALK	*	-122.0	-35.0	6.0	*
37.	RECP LL SIDEWALK	*	-204.0	-35.0	6.0	*
38.	RECP MM SIDEWALK	*	-286.0	-35.0	6.0	*
39.	RECP NN SIDEWALK	*	-600.0	22.0	6.0	*
40.	RECP OO SIDEWALK	*	-286.0	25.0	6.0	*
41.	RECP PP SIDEWALK	*	-204.0	25.0	6.0	*
42.	RECP QQ SIDEWALK	*	-122.0	25.0	6.0	*
43.	RECP RR SIDEWALK	*	-40.0	30.0	6.0	*
44.	RECP SS SIDEWALK	*	-22.0	-122.0	6.0	*
45.	RECP TT SIDEWALK	*	-22.0	-204.0	6.0	*
46.	RECP UU SIDEWALK	*	-22.0	-286.0	6.0	*
47.	RECP VV SIDEWALK	*	-42.0	600.0	6.0	*

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

DATE : 1/22/13
TIME : 12:57:45

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
48. RECP WW SIDEWALK	42.0	600.0	6.0
49. RECP XX SIDEWALK	35.0	286.0	6.0
50. RECP YY SIDEWALK	35.0	204.0	6.0
51. RECP ZZ SIDEWALK	45.0	122.0	6.0

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
5.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
10.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
15.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
20.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
25.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
30.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
35.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
40.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
45.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
50.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
55.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
60.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
65.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
70.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
75.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
80.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
85.	0.	0.	0.	1.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
90.	0.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	0.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	0.
105.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	0.
110.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.	1.	0.	0.	0.	1.	0.
115.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
125.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
130.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
135.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
140.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
145.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
150.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.
155.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.

160.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
165.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.
170.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
175.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
180.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
185.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
190.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
195.	*	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
200.	*	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
205.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND * CONCENTRATION
ANGLE * (ug/m**3)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
210. *	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
215. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
220. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
225. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
230. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
235. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
240. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
245. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
250. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
255. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
260. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
265. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
270. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
275. *	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
280. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
285. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
290. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
295. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
300. *	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
305. *	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
310. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
315. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
320. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
325. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
330. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
335. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
340. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
345. *	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
350. *	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
355. *	0.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.
MAX *	0.	1.	1.	1.	1.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	1.	2.
DEGR. *	235	345	350	55	10	5	15	30	60	75	55	60	110	120	105	115	100	95	20	345

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40	REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210. *																															
215. *																															
220. *																															
225. *																															
230. *																															
235. *																															
240. *																															
245. *																															
250. *																															
255. *																															
260. *																															
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290. *																															
295. *																															
300. *																															
305. *																															
310. *																															
315. *																															
320. *																															
325. *																															
330. *																															
335. *																															
340. *																															
345. *																															
350. *																															
355. *																															
MAX *																															
DEGR. *																															

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
5.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
25.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
35.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
55.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
60.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
65.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
70.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
75.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
85.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.
90.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.
95.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.
100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
105.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
115.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
125.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
135.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
145.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
155.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.

160.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	1.
165.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	1.
170.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
175.	*	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
180.	*	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.
185.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
190.	*	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
195.	*	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
200.	*	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
205.	*	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
210.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
215.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
220.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
225.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
230.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
235.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
240.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
245.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
250.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
255.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
260.	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
265.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
270.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	1.
275.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
280.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
285.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
290.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
295.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
300.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
305.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
310.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
315.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
320.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.
325.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
330.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
335.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
340.	1.	1.	0.	0.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
345.	1.	0.	0.	0.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
350.	1.	0.	0.	0.	2.	1.	0.	2.	2.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
355.	0.	0.	0.	0.	2.	0.	0.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
MAX	1.	1.	1.	0.	2.	1.	1.	2.	2.	1.	2.	2.	2.	1.	1.	1.	1.	1.	1.	1.
DEGR.	265	270	265	260	345	275	275	350	350	355	10	10	5	5	5	25	25	65	95	105

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
0.	0.	0.	1.	2.	2.	2.	1.	1.	1.	1.	1.
5.	0.	1.	2.	2.	2.	2.	1.	0.	1.	1.	1.
10.	0.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.
15.	1.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.
20.	1.	1.	2.	2.	1.	1.	2.	0.	0.	0.	0.
25.	1.	1.	2.	1.	1.	1.	1.	0.	0.	0.	0.
30.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
35.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
40.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
45.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
50.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
55.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
60.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
65.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
70.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
75.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
80.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
85.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
90.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
95.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
100.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
105.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
110.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
115.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
120.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
125.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
130.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
135.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
140.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
145.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
150.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
155.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.

160.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
165.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
170.	*	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.
175.	*	1.	1.	1.	1.	1.	1.	2.	1.	1.	1.	0.
180.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
185.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
190.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.	1.
195.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.	1.
200.	*	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.
205.	*	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.

JOB: LLOYD WINERY PROPERTY CAL3QHC ANAL.21 RUN: LLOYD WINERY PROP PM 21 BLD, NW SIDE

WIND ANGLE RANGE: 0.-355.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51
210.	1.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.
215.	1.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.
220.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
225.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
230.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
235.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
240.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
245.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
250.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
255.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
260.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
265.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
270.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.
275.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
280.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
285.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
290.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
295.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
300.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
305.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
310.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
315.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
320.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
325.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
330.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.
335.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.
340.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.
345.	0.	0.	0.	0.	1.	0.	0.	2.	2.	2.	2.
350.	0.	0.	0.	1.	1.	1.	0.	2.	2.	2.	2.
355.	0.	0.	1.	1.	1.	1.	1.	1.	2.	2.	1.
MAX	1.	1.	2.	2.	2.	2.	2.	2.	2.	2.	2.
DEGR.	125	120	10	5	5	0	170	190	345	345	345

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC45.